# EE540 Advance Electromagnetic Theory & Antennas

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#### Polarization

- Let us consider antenna is placed at the origin of a spherical coordinate system
  - and wave is propagating radially outward in all directions
- In the far field region of an antenna, the electric field of the antenna is given by

$$\vec{E}(\theta,\phi) = E_{\theta}(\theta,\phi)\hat{\theta} + E_{\phi}(\theta,\phi)\hat{\phi}$$

• Putting the time dependence, we have,

 $\vec{E}(\theta,\phi,t) = E_{\theta}(\theta,\phi)\cos(\omega t)\hat{\theta} + E_{\phi}(\theta,\phi)\cos(\omega t + \delta)\hat{\phi} = E_{\theta}(\theta,\phi,t)\hat{\theta} + E_{\phi}(\theta,\phi,t)\hat{\phi}$ 

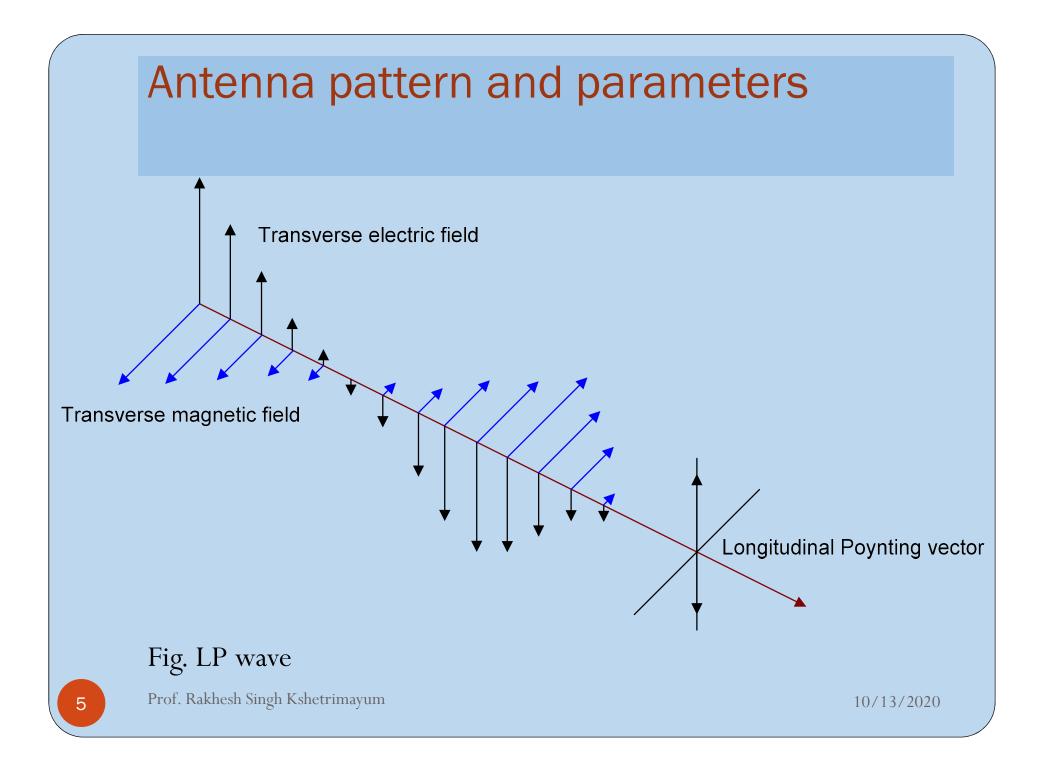
- where  $\delta$  is the phase difference between the elevation and azimuthal components of the electric field
- The figure traced out by the tip of the radiated electric field vector
  - as a function of time for a fixed position of space can be defined as antenna polarization

#### a) LP

- When  $\delta=0$ , the two transversal electric field components are in time phase
- The total electric field vector
- $\vec{E}(\theta, \phi, t) = E_{\theta}(\theta, \phi) cos \omega t \hat{\theta} + E_{\phi}(\theta, \phi) cos \omega t \hat{\phi}$
- makes an angle  $heta_{LP}$  with the heta-axis

$$\theta_{LP} = tan^{-1} \left[ \frac{E_{\theta}(\theta, \phi, t)}{E_{\phi}(\theta, \phi, t)} \right] = tan^{-1} \left[ \frac{E_{\theta}(\theta, \phi)}{E_{\phi}(\theta, \phi)} \right]$$

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- The tip of the total radiated electric field vector traces out a line
- Therefore, the antenna's polarization is LPb) CP

• When 
$$\delta = \pm \frac{\pi}{2}$$
,

- the two transversal electric field components are out of phase in time
- and if the two transversal electric field components are of equal amplitude  $E_{\theta}(\theta, \phi) = E_{\phi}(\theta, \phi) = E_{0}(\theta, \phi)$

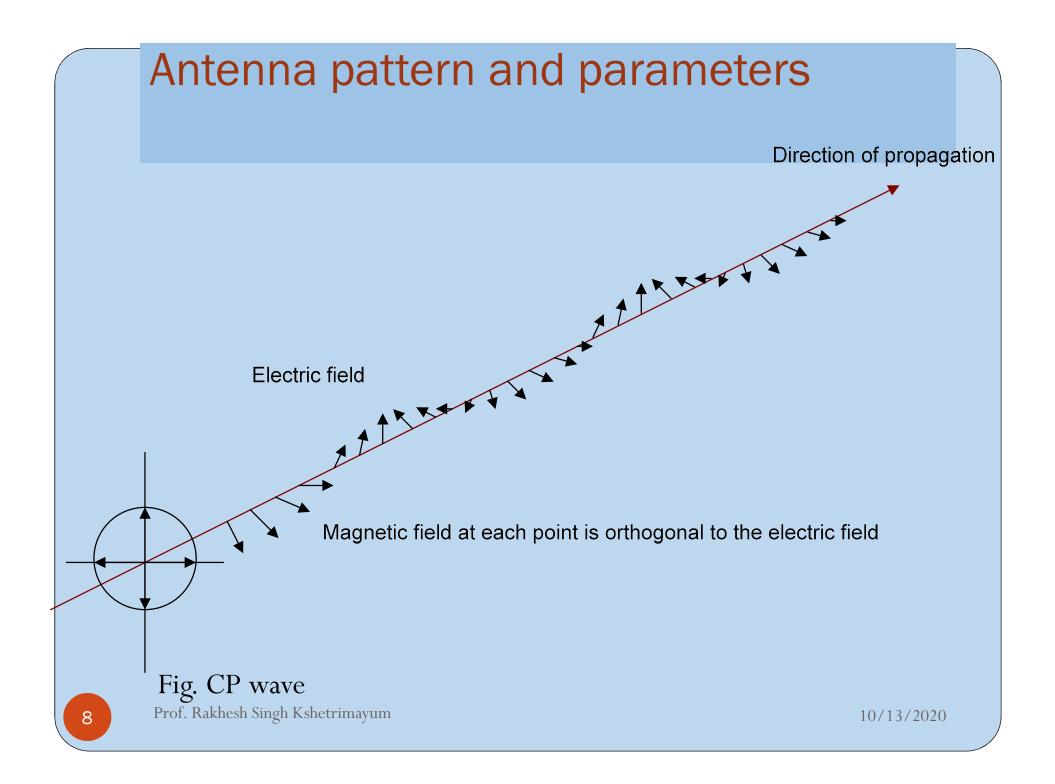
- The total electric field vector
- $\vec{E}(\theta,\phi,t) = E_{\theta}(\theta,\phi)cos\omega t\hat{\theta} + E_{\phi}(\theta,\phi)cos\left(\omega t \pm \frac{\pi}{2}\right)\hat{\phi}$
- $\vec{E}(\theta, \phi, t) = E_{\theta}(\theta, \phi) cos \omega t \hat{\theta} \mp E_{\phi}(\theta, \phi) sin(\omega t) \hat{\phi}$
- makes an angle  $heta_{CP}$  with the heta-axis

• 
$$\theta_{CP} = tan^{-1} \left[ \mp \frac{sin\omega t}{cos\omega t} \right] = tan^{-1} [\mp tan\omega t] = \mp \omega t$$

- This implies that the total radiated electric field vector of the antenna traces out a circle as time progresses from 0 to  $2\frac{\pi}{\omega}$  and so on
- If the vector rotates counterclockwise for which  $\theta_{CP}$  is positive (clockwise for which  $\theta_{CP}$  is negative), then the antenna polarization is RHCP (LHCP)



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- The total electric field vector for CP can be also expressed as
- $\vec{E}(\theta,\phi,t) = Re\left\{E_0(\theta,\phi)e^{j\omega t}\hat{\theta} + E_0(\theta,\phi)e^{j\left(\omega t \pm \frac{\pi}{2}\right)}\hat{\phi}\right\}$
- For RHCP,
- $\vec{E}(\theta,\phi,t) = Re\left\{E_0(\theta,\phi)e^{j\omega t}\hat{\theta} + E_0(\theta,\phi)e^{j\left(\omega t \frac{\pi}{2}\right)}\hat{\phi}\right\}$
- $\vec{E}(\theta,\phi,t) = Re\left[E_0(\theta,\phi)e^{j\omega t}\left\{\hat{\theta} + e^{j\left(-\frac{\pi}{2}\right)}\hat{\phi}\right\}\right]$
- $\vec{E}(\theta,\phi,t) = Re[E_0(\theta,\phi)e^{j\omega t}\{\hat{\theta}-j\hat{\phi}\}]$
- For LHCP,
- $\vec{E}(\theta,\phi,t) = Re\left\{E_0(\theta,\phi)e^{j\omega t}\hat{\theta} + E_0(\theta,\phi)e^{j\left(\omega t + \frac{\pi}{2}\right)}\hat{\phi}\right\}$
- $\vec{E}(\theta, \phi, t) = Re[E_0(\theta, \phi)e^{j\omega t}\{\hat{\theta} + j\hat{\phi}\}]$

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- The total electric field vector for CP in Cartesian coordinates assuming wave propagation along z-axis can be also expressed as
- $\vec{E} = Re\left\{E_0e^{j\omega t}\hat{x} + E_0e^{j\left(\omega t \pm \frac{\pi}{2}\right)}\hat{y}\right\}$
- For RHCP,
- $\vec{E} = Re\left\{E_0e^{j\omega t}\hat{x} + E_0e^{j\left(\omega t \frac{\pi}{2}\right)}\hat{y}\right\}$
- $\vec{E} = Re\left[E_0e^{j\omega t}\left\{\hat{x} + e^{j\left(-\frac{\pi}{2}\right)}y\right\}\right]$
- $\vec{E} = Re[E_0e^{j\omega t}\{\hat{x} j\hat{y}\}]$
- For unit vectors for RHCP can be expressed as  $\hat{e} = \frac{1}{\sqrt{2}} \{\hat{x} j\hat{y}\}$
- For unit vectors for LHCP can be expressed as  $\hat{e} = \frac{1}{\sqrt{2}} \{\hat{x} + j\hat{y}\}$ Prof. Rakhesh Singh Kshetrimayum

• For  $E_{\theta}(\theta, \phi) \neq E_{\phi}(\theta, \phi)$  and  $\delta \neq 0, \pi$ 

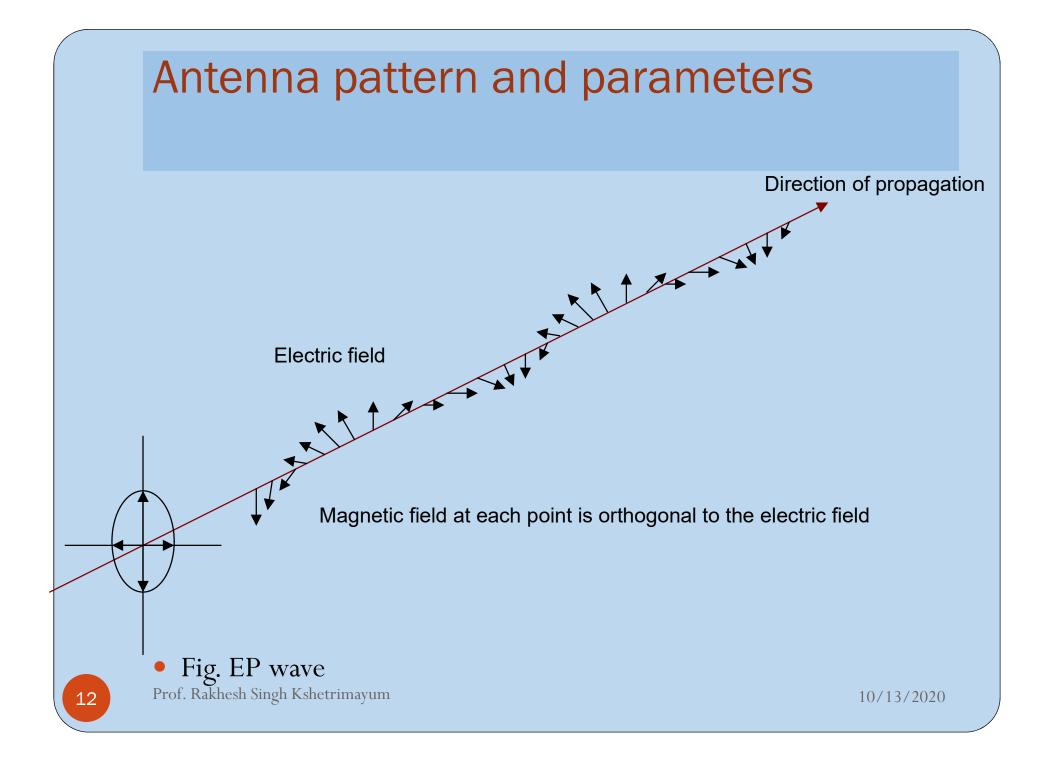
• the total electric field vector traces out an ellipse and

- hence it is elliptically polarized (EP)  $\vec{E}_{EP} = \left(\hat{\theta} + Ae^{j\delta}\hat{\phi}\right)e^{-j\beta r}e^{j\omega t}$
- Unit vector for EP,  $\vec{e} = \frac{\widehat{\theta} + Ae^{j\delta}\widehat{\phi}}{\sqrt{1+A^2}}$
- If  $\delta$  is in the upper half of the complex plane, LHEP and vice versa LP  $(\delta = 0, \pi)$ , RHCP  $(A = 1, \delta = -\frac{\pi}{2})$ & LHCP  $(A = 1, \delta = \frac{\pi}{2})$

• The ratio of the major and minor axes of the ellipse is called axial ratio (AR)

• For instance, AR=0 dB for CP and AR=  $\infty$  dB for LP





- Antenna polarization:
- To sum up,
- The polarization of a radiated wave in the far field region of an antenna defines antenna polarization
- Assume a transmitting antenna transmitting electric field of maximum magnitude  $E_m$  in the far field region of an antenna

$$\vec{E}^t = E_m \hat{e}_t$$

• where  $\hat{e}_t$  is the unit vector which gives polarization for the transmitting antenna

- It is the complex vector representation of field normalized to unity
- Assume that there is a receiving antenna in the far field region of this antenna
- The field of some magnitude E<sup>m</sup> that would give maximum received power at the received antenna terminal is

$$\vec{E}^r = E^m \hat{e}_r$$

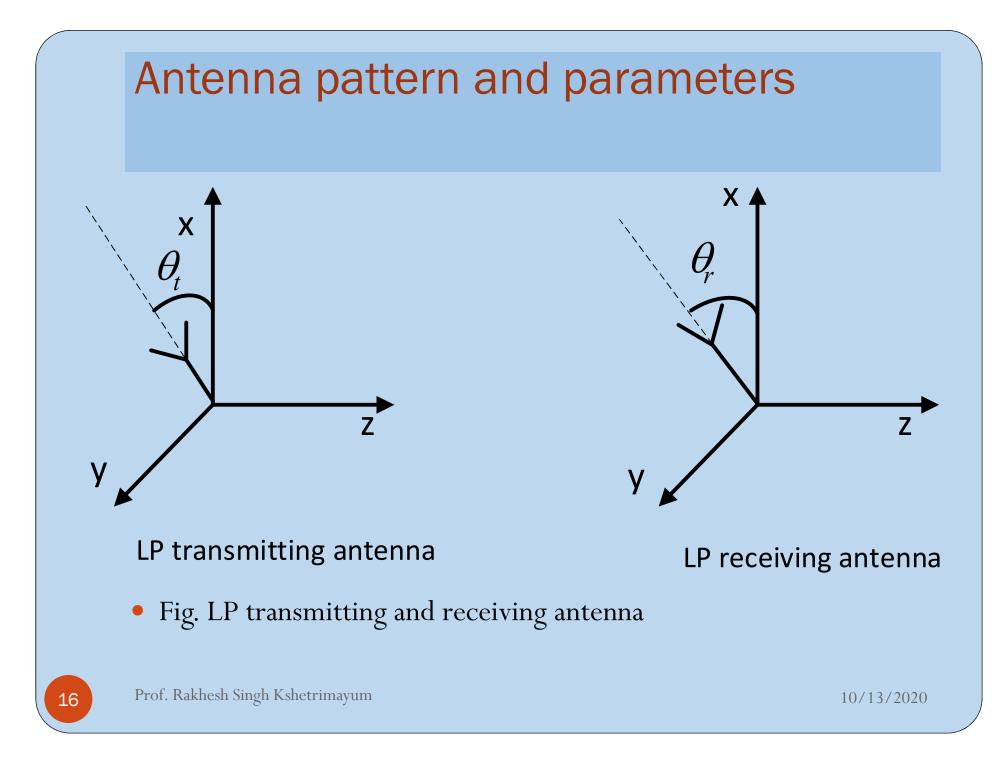
• where  $\hat{e}_r$  is the unit vector which gives polarization for the receiving antenna

• Polarization efficiency is defined as

$$P.E. = \left| \hat{e}_t \bullet \hat{e}_r^* \right|^2$$

- Receiving LP wave with an LP receiving antenna:
- Let us consider a case where the transmitting antenna is placed at an angle  $\theta_t$  w.r.t x-axis
- and the receiving antenna is placed at an angle  $\theta_{\rm r}$  w.r.t x-axis
- Both transmitting and receiving antennas are LP antennas (assume wave propagation along z-axis)





• Therefore, polarization unit vectors for the transmitting and receiving antennas are

$$\hat{e}_t = \cos \theta_t \hat{x} + \sin \theta_t \hat{y}; \hat{e}_r = \cos \theta_r \hat{x} + \sin \theta_r \hat{y}$$

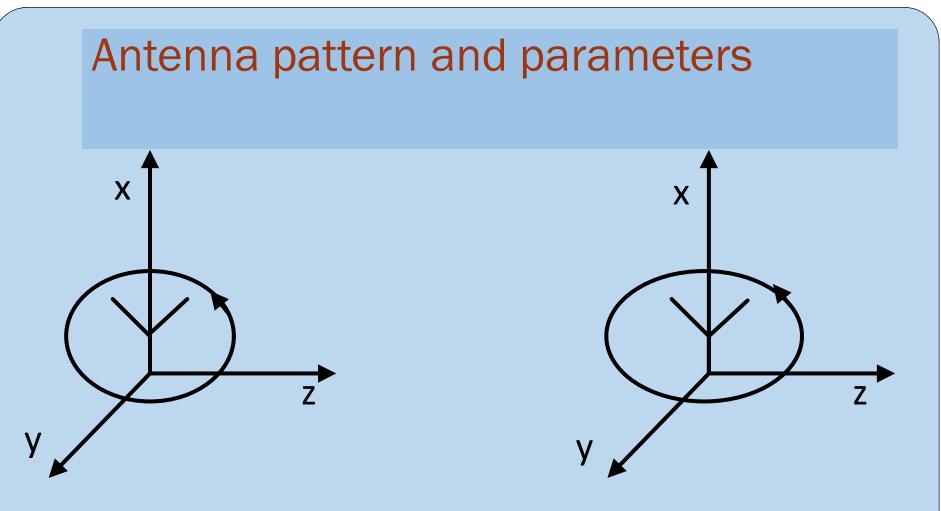
• Polarization efficiency can be calculated as

$$P.E. = \left| \hat{e}_t \bullet \hat{e}_r^* \right|^2 = \cos^2(\theta_t - \theta_r)$$
$$\theta_t - \theta_r$$

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$\theta_t - \theta_r$	<b>P.E.</b>	Illustration
0	1	YY
π/2	0	$\mathbf{Y}$
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#### **RHCP** transmitting antenna

**RHCP** receiving antenna

• Fig. Receiving a CP wave with a CP receiving antenna

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- Receiving a CP wave with a CP receiving antenna
- Consider a RHCP receiving antenna is kept in the far field region of RHCP transmitting antenna
- Assume wave propagation along positive z-axis
- Hence the polarization unit vectors for transmitting and receiving antennas are

$$\hat{e}_t = \frac{1}{\sqrt{2}} \left( \hat{x} - j\hat{y} \right); \hat{e}_r = \frac{1}{\sqrt{2}} \left( \hat{x} - j\hat{y} \right)$$

• Polarization efficiency

$$P.E. = \left| \hat{e}_t \bullet \hat{e}_r^* \right|^2 = 1$$

• For instance, the receiving antenna is LHCP

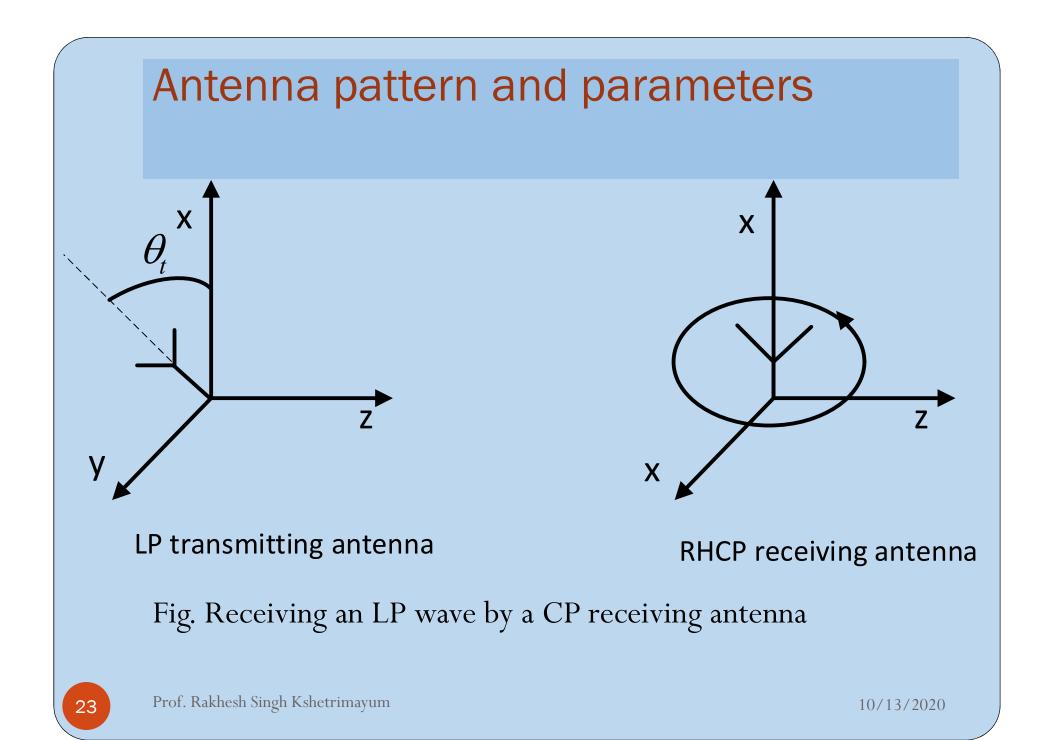
$$\hat{e}_t = \frac{1}{\sqrt{2}} \left( \hat{x} - j\hat{y} \right); \hat{e}_r = \frac{1}{\sqrt{2}} \left( \hat{x} + j\hat{y} \right)$$

• Polarization efficiency

$$P.E. = \left| \hat{e}_t \bullet \hat{e}_r^* \right|^2 = 0$$

- It is like two persons shaking hands
- Right to right hand shake is matched but right to left hand shake is not matched
- Receiving an LP wave by a CP receiving antenna:
- Consider an LP wave transmitting antenna which is oriented at an angle  $\theta_t$  with the x-axis
- Receiving antenna is a RHCP antenna
- Hence

$$\hat{e}_t = \cos\theta_t \hat{x} + \sin\theta_t \hat{y}; \hat{e}_r = \frac{1}{\sqrt{2}} (\hat{x} - j\hat{y})$$



- Therefore
- Polarization efficiency is

$$P.E. = \left| \hat{e}_t \bullet \hat{e}_r^* \right|^2 = \frac{1}{2} \left| \cos \theta_t + j \sin \theta_t \right|^2 = \frac{1}{2}$$

- Hence there is a 3-dB signal loss
- The same case when one use a RHCP/LHCP transmitting antenna and a LP receiving antenna

- Let us try to understand two terms (co- and crosspolarization) which are important for the antenna radiation pattern
- Co-polarization means you measure the antenna with another antenna oriented
  - in the same polarization with the antenna under test (AUT)
- Cross-polarization means that you measure the antenna with antenna oriented
  - perpendicular w.r.t. the main polarization

- Cross-polarization is the polarization orthogonal
  - to the polarization under consideration
- For example,
  - if the field of an antenna is horizontally polarized,
  - the cross-polarization for this case is vertical polarization
- If the polarization is RHCP,
  - the cross-polarization is LHCP
- Let us put this into mathematical expressions:
- We may write the total electric field propagating along z-axis as  $\vec{E} = (E_{co}\hat{u}_{co} + E_{cr}\hat{u}_{cr})e^{-j\beta z}$

• where the co- and cross-polarization unit vectors satisfy the orthonormality condition

$$\hat{u}_{co} \bullet \hat{u}_{co}^* = 1, \hat{u}_{cr} \bullet \hat{u}_{cr}^* = 1, \hat{u}_{co} \bullet \hat{u}_{cr}^* = 0, \hat{u}_{cr} \bullet \hat{u}_{co}^* = 0$$

- Therefore,
- the co- and cross-polarization components of the electric fields can be obtained as

$$E_{co} = \vec{E} \bullet \hat{u}_{co}^*, E_{cr} = \vec{E} \bullet \hat{u}_{cr}^*$$

#### a) LP

- For a general LP wave along  $\phi_{LP}$ , we can write,  $\hat{u}_{co} = \cos \phi_{LP} \hat{x} + \sin \phi_{LP} \hat{y}, \hat{u}_{cr} = \sin \phi_{LP} \hat{x} - \cos \phi_{LP} \hat{y}$
- For a x-directed LP wave,  $\phi_{LP} = 0$ , hence,

$$\hat{u}_{co} = \hat{x}, \hat{u}_{cr} = -\hat{y}; E_{co} = \vec{E} \bullet \hat{u}_{co}^* = E_x, E_{cr} = \vec{E} \bullet \hat{u}_{cr}^* = -E_y$$

• For a y-directed LP wave,  $\phi_{LP} = 90^{\circ}$ , hence,

$$\hat{u}_{co} = \hat{y}, \hat{u}_{cr} = \hat{x}; E_{co} = \vec{E} \bullet \hat{u}_{co}^* = E_y, E_{cr} = \vec{E} \bullet \hat{u}_{cr}^* = E_x$$

#### b) CP

• For a RHCP wave propagating along z-axis, we can write,

$$\hat{u}_{co} = \frac{\hat{x} - j\hat{y}}{\sqrt{2}}, \hat{u}_{cr} = \frac{\hat{x} + j\hat{y}}{\sqrt{2}}$$

$$E_{co} = \vec{E} \bullet \hat{u}_{co}^* = \frac{E_x + jE_y}{\sqrt{2}}, E_{cr} = \vec{E} \bullet \hat{u}_{cr}^* = \frac{E_x - jE_y}{\sqrt{2}}$$

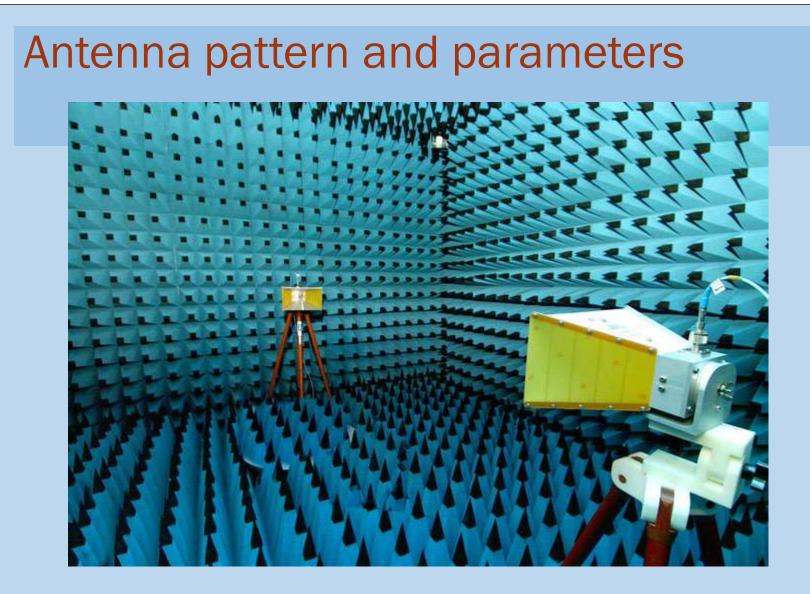
• For a LHCP wave, co- and cross-polarization unit vectors and components of the electric field will interchange

#### c) EP

• For a EP wave, we can write,

$$\hat{u}_{co} = \frac{\hat{x} + Ae^{j\phi_{EP}}\hat{y}}{\sqrt{1 + A^2}}, \\ \hat{u}_{cr} = \frac{-Ae^{-j\phi_{EP}}\hat{x} + \hat{y}}{\sqrt{1 + A^2}}$$

- In order to determine the far-field radiation pattern of an AUT, two antennas are required
- The one being tested (AUT) is normally free to rotate and it is connected in receiving mode



#### Fig. Antenna measurement set up

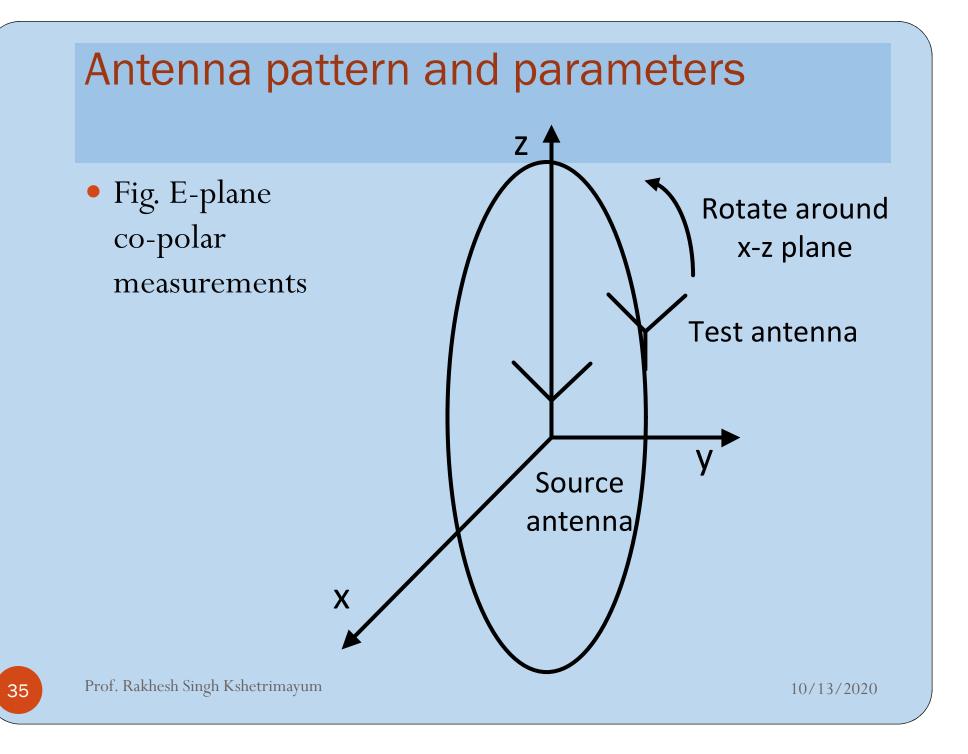
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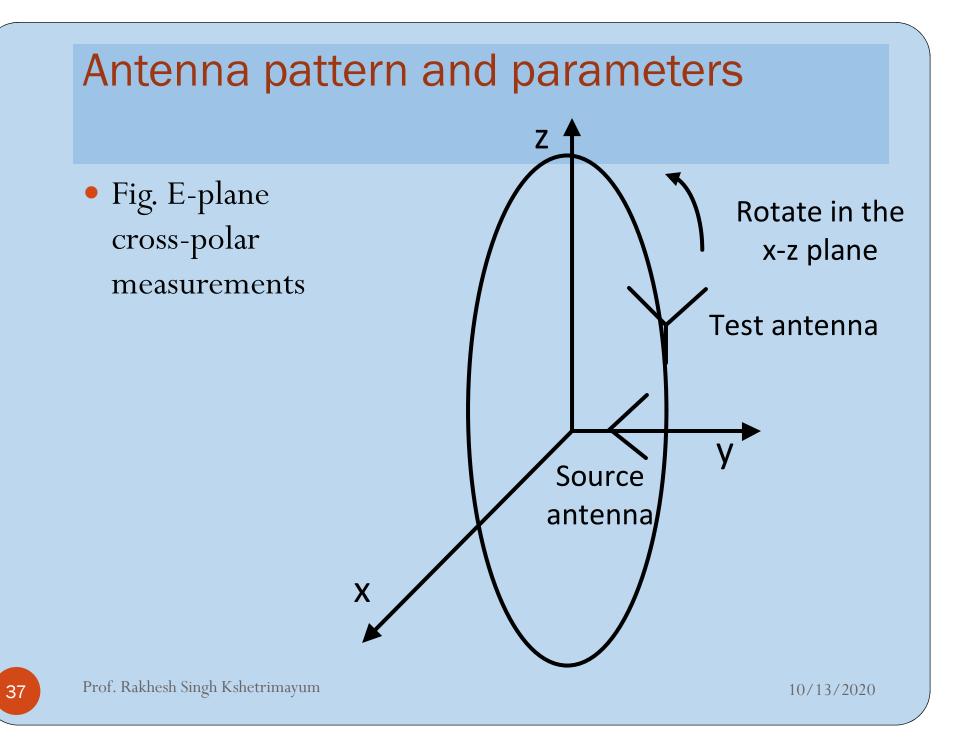
- Note that AUT as a receiving antenna measurement will generate the same radiation pattern
  - to that of AUT used as a transmitting antenna
- Another antenna is usually fixed and it is connected in transmitting mode
- The AUT is rotated by a positioner and
  - it can rotate 1-, 2- and 3-degrees of freedom of rotation

- The AUT is rotated in usually two principal planes (elevation and azimuthal)
- The received field strength is measured by a spectrum analyzer or power meter
  - which will be used to generate the antenna radiation pattern in two principal planes also known as E- and H- planes
- The antenna radiation patterns in these two principal planes can be used to generate the 3-D radiation pattern of an antenna

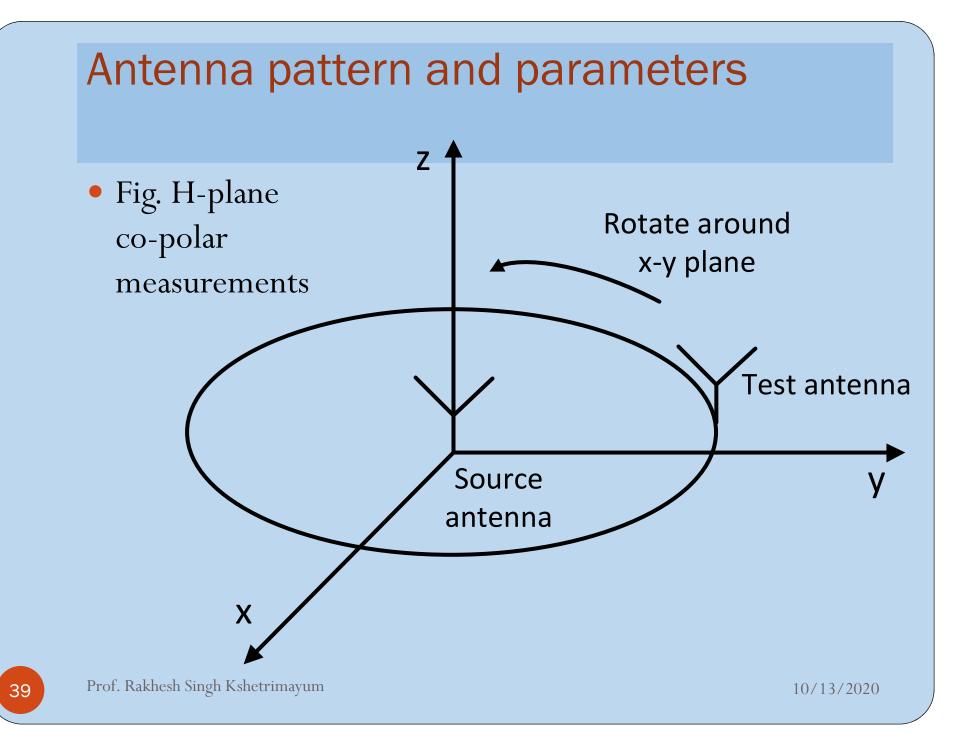
- Let us consider Hertz dipole which is a vertically polarized antenna
- For E-plane **co-polar measurements**,
  - source and test antenna are oriented vertically
  - so that the main beam of the test antenna (receiving antenna) is directed towards y-axis
- Source antenna is kept stationary and
  - we rotate the test antenna in the x-z plane
  - ullet and record the electric fields variation over ullet



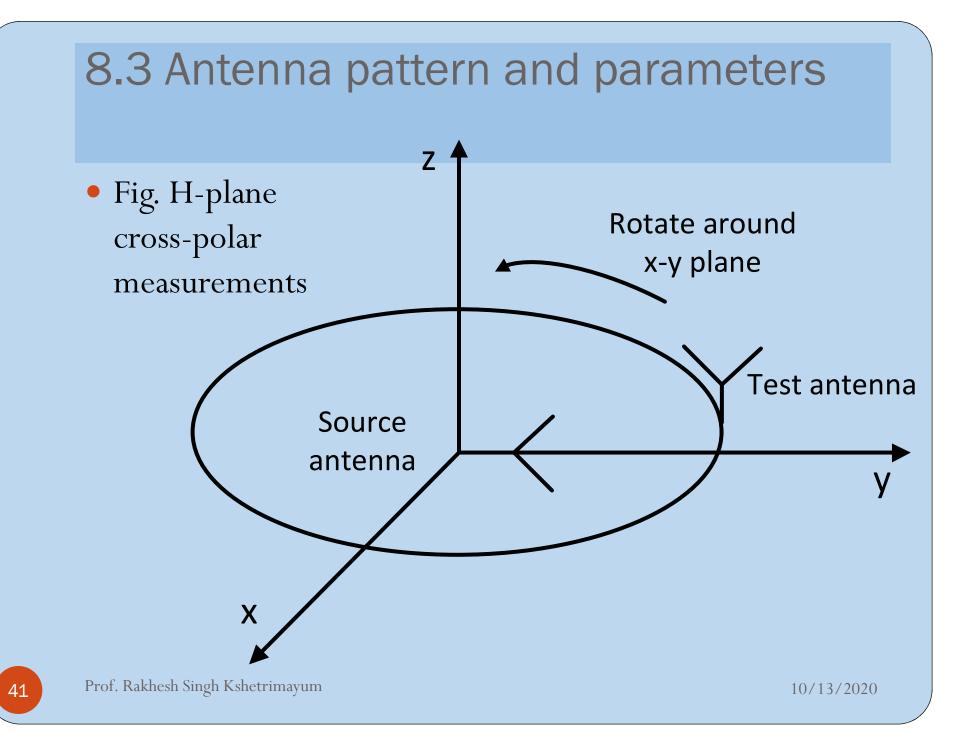
- For E-plane cross-polar measurements,
  - source is oriented horizontally and test antenna is oriented vertically
- Source antenna is kept stationary and
  - we rotate the test antenna in the x-z plane
  - ullet and record the electric fields variation over ullet

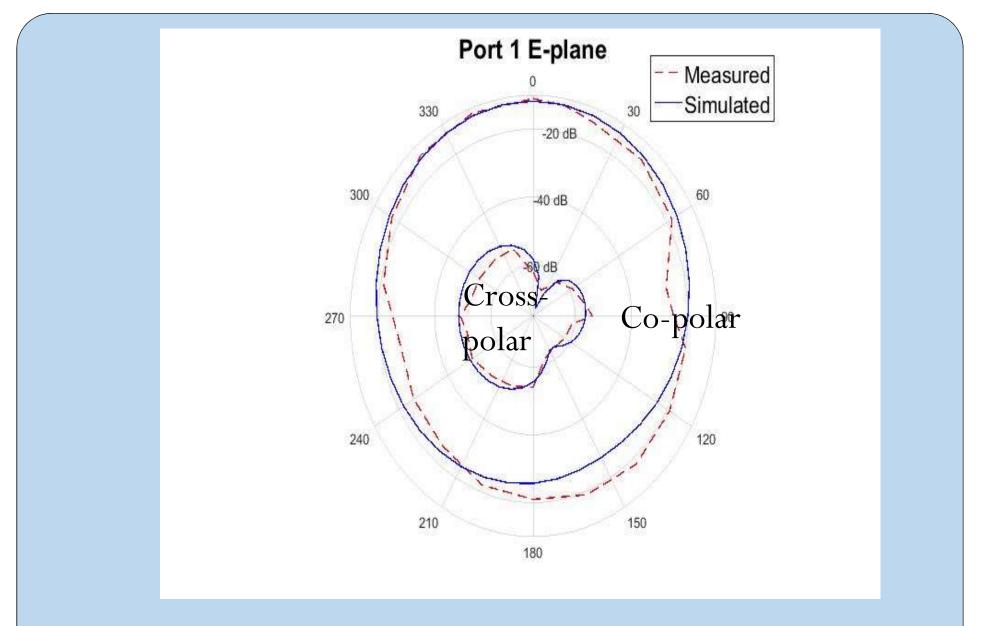


- For H-plane **co-polar measurements**,
  - source and test antenna are oriented vertically
- Source antenna is kept stationary and
  - we rotate the test antenna in the x-y plane
  - $\bullet$  and record the electric fields variation over  $\phi$



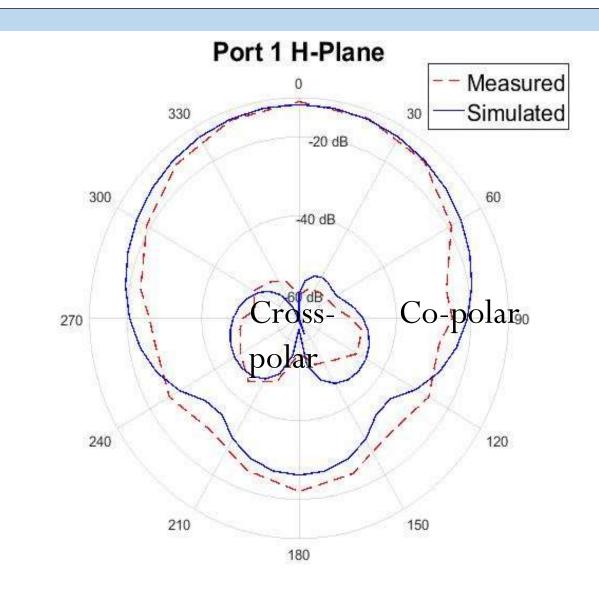
- For H-plane cross-polar measurements,
  - source is oriented horizontally and test antenna is oriented vertically
- Source antenna is kept stationary and
  - we rotate the test antenna in the x-y plane
  - $\bullet$  and record the electric fields variation over  $\phi$





#### Fig. Typical E-plane pattern

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#### Fig. Typical H-plane pattern

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- Let us look at the antenna input characteristics
- Antenna is considered as a load to the transmission line
- Hence one can find out the equivalent circuit of an antenna
- Antenna is a resonator
- It can be equivalently modelled as a series RLC circuit (simplest model)

#### Quality factor and bandwidth

- The equivalent circuit of a resonant antenna can be
  - approximated by a series RLC resonant circuit
  - where  $R = R_r + R_L$  are the radiation and loss resistances,
  - L is the inductance and
  - C is the capacitance of the antenna

- For a resonant antenna like dipoles,
  - the FBW is related to the radiation efficiency and quality factor Q (FBW=1/Q)
- The quality factor of an antenna is defined as 2πf<sub>0</sub> (f<sub>0</sub> is the resonant frequency) times the energy stored over the power radiated and Ohmic losses

$$Q = 2\pi f_0 \frac{\frac{1}{4} |I|^2 L + \frac{1}{4} |I|^2 \frac{1}{(2\pi f_0)^2 L}}{\frac{1}{2} |I|^2 (R_r + R_L)} = \frac{2\pi f_0 L}{R_r + R_L} = \frac{1}{2\pi f_0 (R_r + R_L) C}$$
$$= \frac{1}{2\pi f_0 R_r C} \frac{R_r}{(R_r + R_L)} = Q_{lossless} \bullet e_{rad}$$

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- where  $Q_{lossless}$  is the quality factor when the antenna is lossless ( $R_L=0$ ) and
- e<sub>rad</sub> is the antenna radiation efficiency.
- Note that the radiation efficiency of an antenna is defined
  - as the ratio of the power delivered
  - $\bullet$  to the radiation resistance  $R_{\rm r}$  to the power delivered to  $R_{\rm r}$  and  $R_{\rm L}$

$$e_{rad} = \frac{\frac{1}{2} |I|^2 R_r}{\frac{1}{2} |I|^2 (R_r + R_L)} = \frac{R_r}{(R_r + R_L)}$$

- The feed line also has a characteristic impedance  $Z_0$  usually of 50 Ohm
- At the input of the antenna, the impedance seen by the feed line can be assumed as  $Z_L$
- Then the reflection coefficient and VSWR may be calculated as  $\Gamma = \frac{Z_L - Z_0}{VSWP} = \frac{1 + |\Gamma|}{1 + |\Gamma|}$

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}; VSWR = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$
$$0 \le |\Gamma| \le 1, 1 \le VSWR \le \infty$$
$$BW: VSWR \le 2$$

