

EE540 Advance Electromagnetic Theory & Antennas

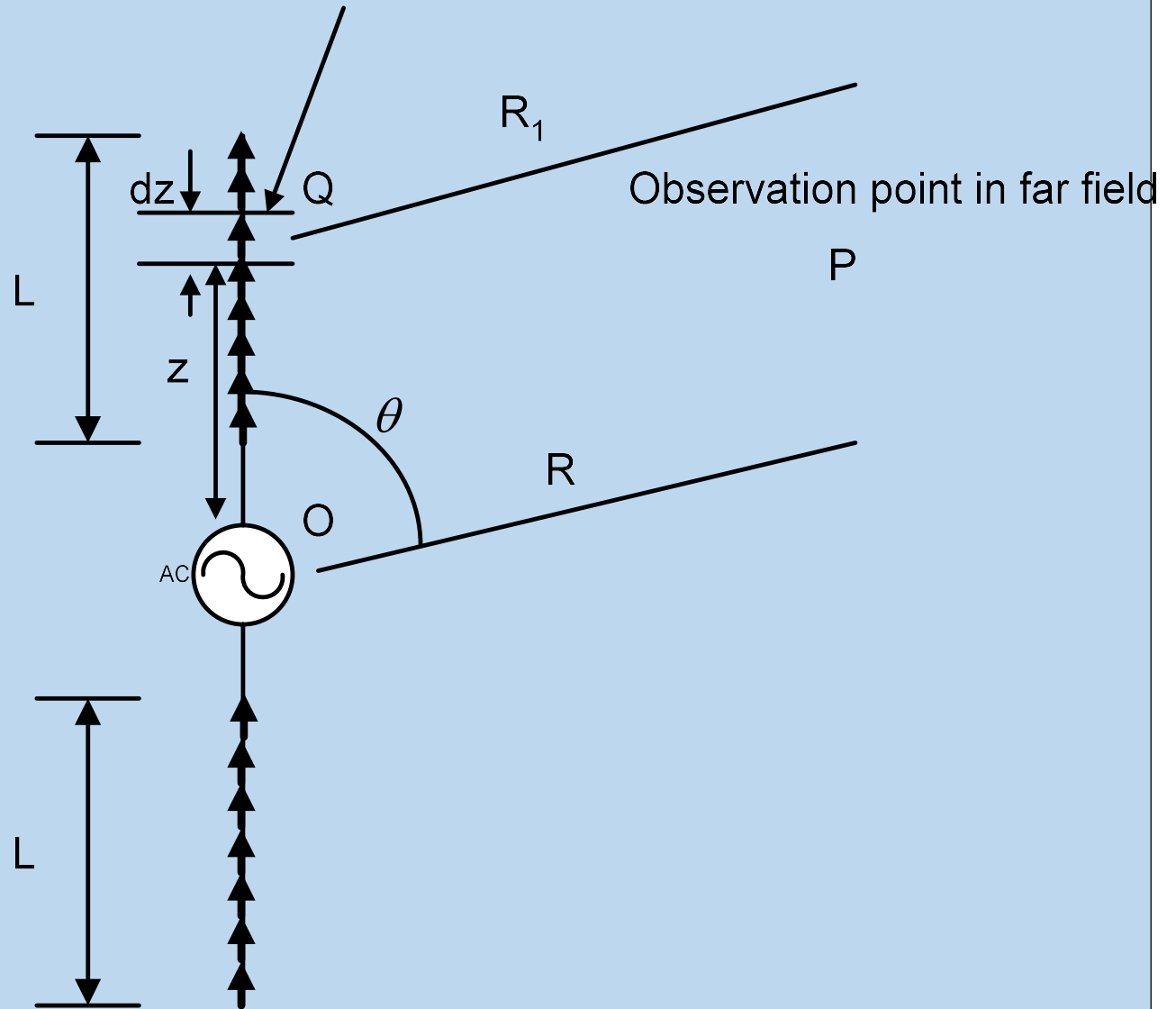
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Kinds of antennas

- **Dipole antenna**
- The next extension of a Hertz dipole is
 - a linear antenna or a dipole of finite length as depicted in Fig.
- It consists of a conductor of length $2L$
 - fed by a voltage or current source at its center
- We will first find the current distribution on such antennas

- Fig. (a) Dipole of length $2L$ (Dipole can be assumed to composed of many Hertz dipoles)

Equivalent to a Hertz dipole of length dz

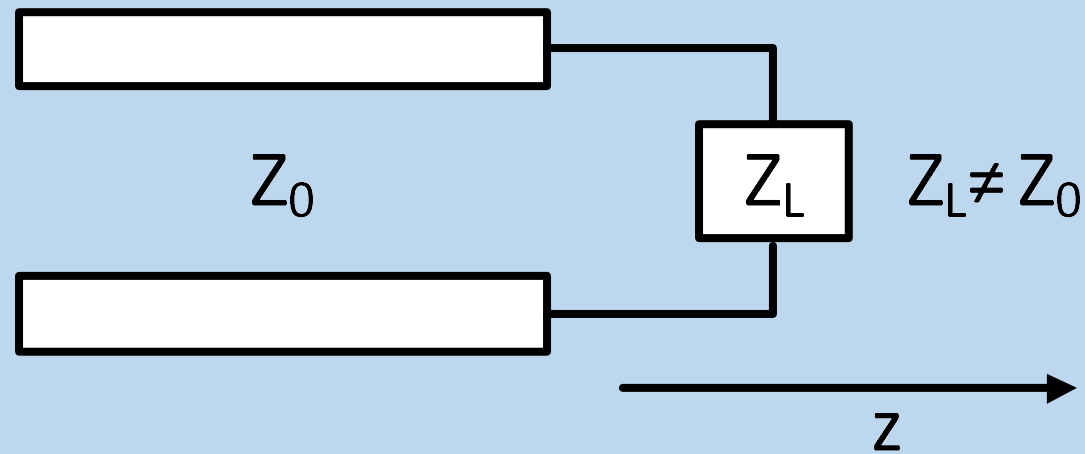


Kinds of antennas

- Let us assume a transmission line loaded with a load Z_L
- Since the line impedance and load impedance may be different
- Any wave incident from the line to the load will be reflected
- Hence at any location along the line,
 - there will be both reflected and incident wave which may be expressed as

$$V(z) = V_0^+ e^{-j\beta z} + V_0^- e^{+j\beta z}$$

Kinds of antennas



- Fig. A transmission line loaded with an impedance of Z_L

Kinds of antennas

- Corresponding electric current wave along the line may be expressed as

$$I(z) = \frac{V_0^+}{Z_0} e^{-j\beta z} - \frac{V_0^-}{Z_0} e^{+j\beta z} = \frac{V_0^+}{Z_0} (e^{-j\beta z} - \Gamma e^{+j\beta z}); \Gamma = \frac{V_0^-}{V_0^+} = \frac{Z_L - Z_0}{Z_L + Z_0}$$

- The characteristic impedance of the line is defined as

$$Z_0 = \frac{V_0^+}{I_0^+} = -\frac{V_0^-}{I_0^-}$$

- For o.c. transmission line

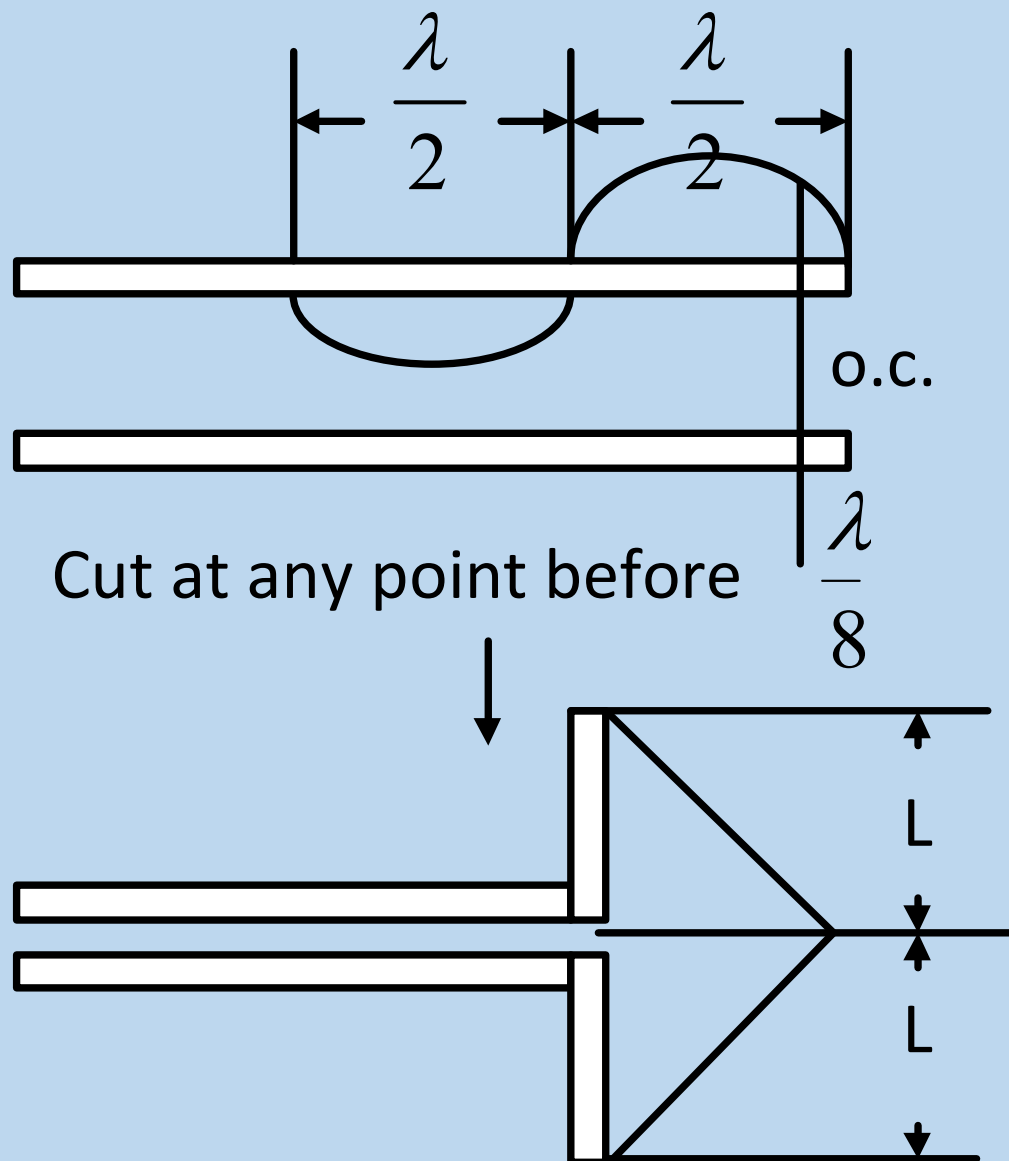
$$I(z) = \frac{V_0^+}{Z_0} (e^{-j\beta z} - e^{+j\beta z}) = -2j \frac{V_0^+}{Z_0} \sin \beta z$$

Kinds of antennas

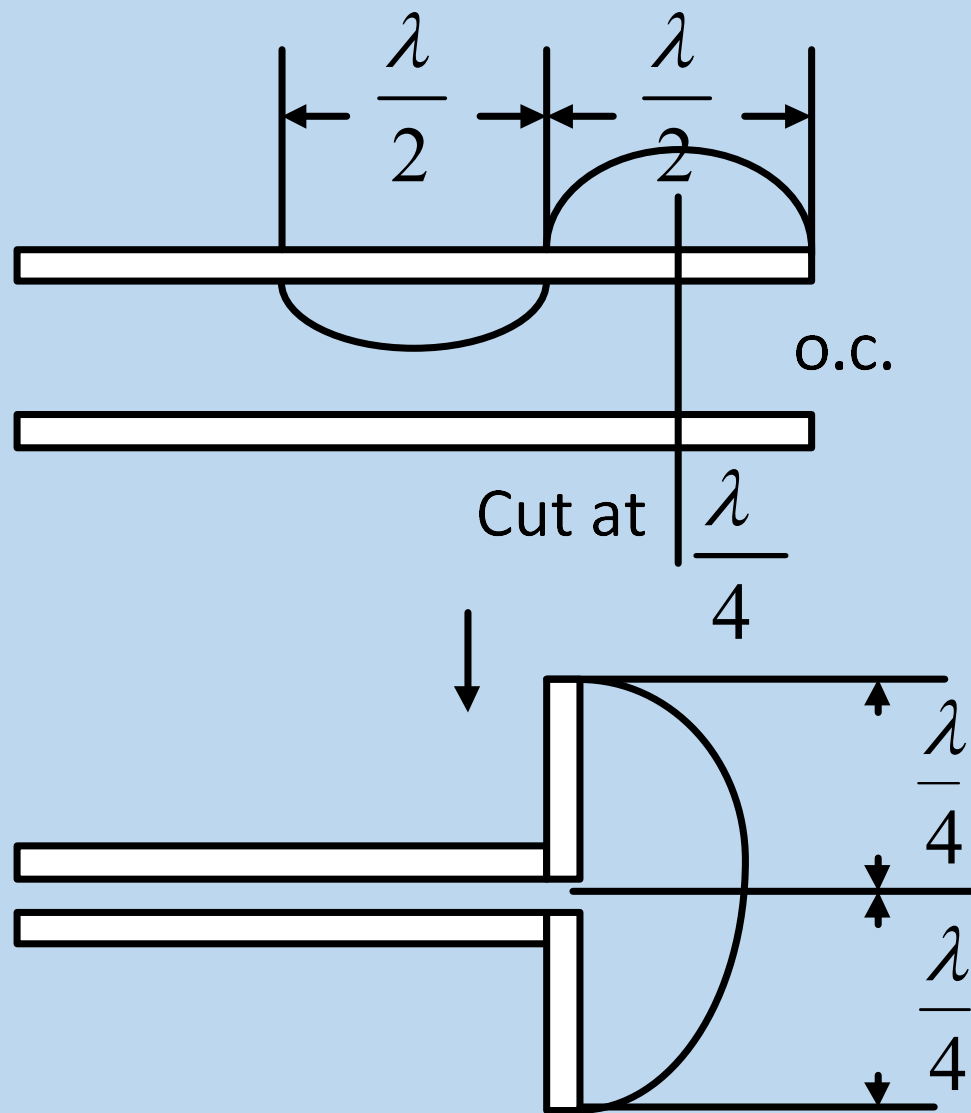
- The current is zero at $z = \pm L$
- since at the ends, there is no path for the current to flow
 - so, we can write,

$$I(z) = -2j \frac{V_0^+}{Z_0} \sin(\beta(L - |z|)) = I_0 \sin[\beta(L - |z|)]; I_0 = -2j \frac{V_0^+}{Z_0}$$

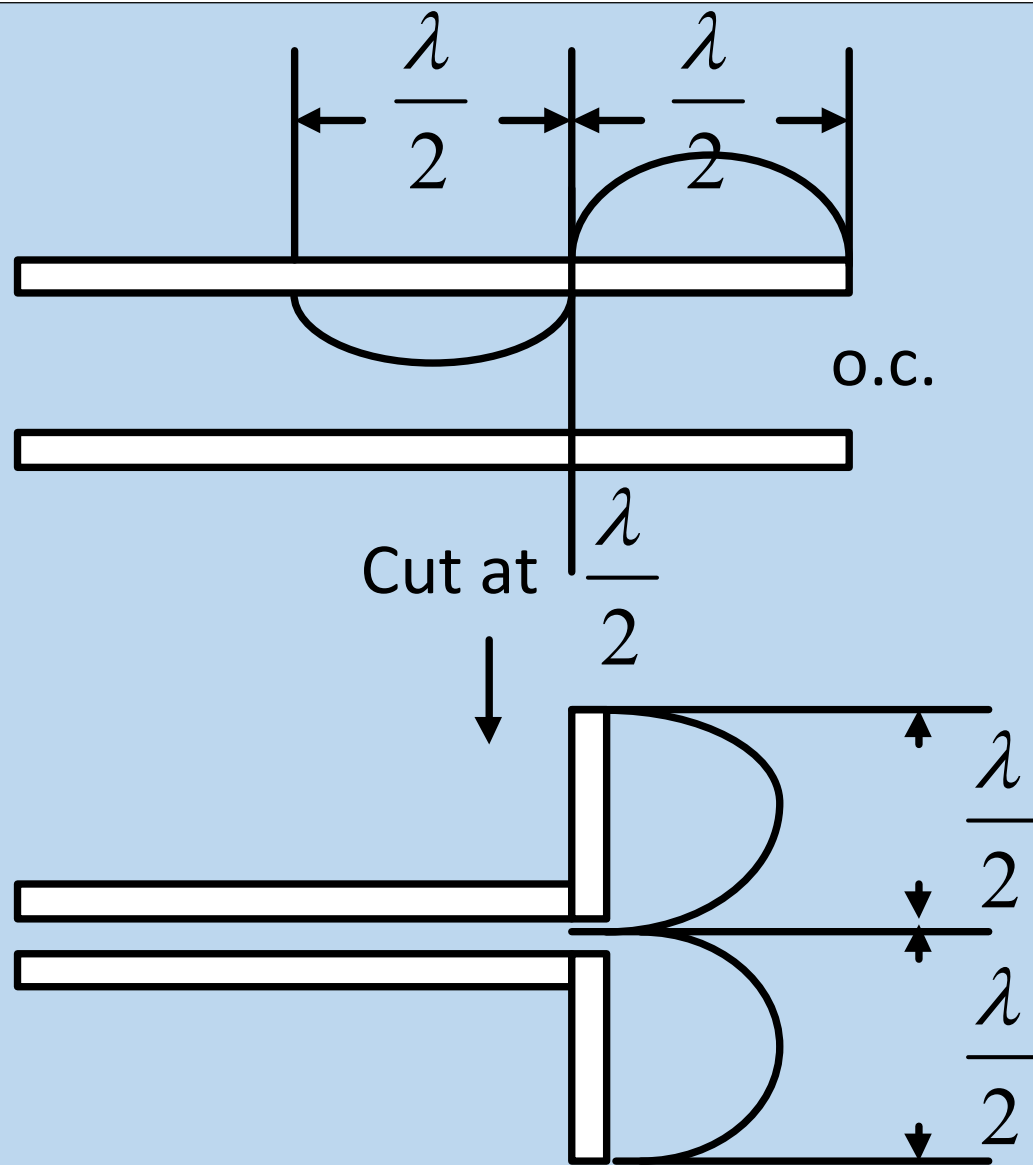
- How to plot the current distribution of dipoles of various length?



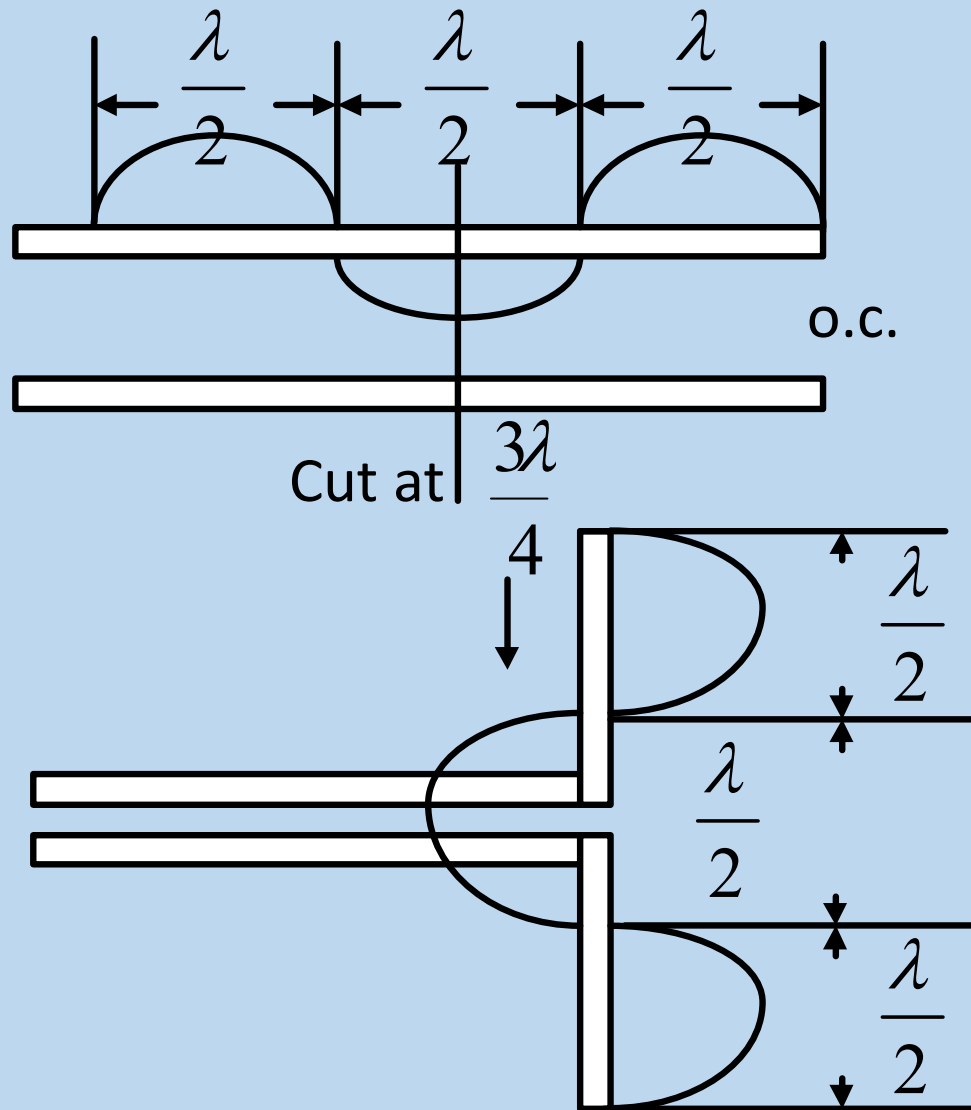
• Fig. Current distribution of a $2L \ll \lambda$ dipole & $L < \lambda/8$



• Fig. Current distribution of a $\lambda/2$ dipole



• Fig. Current distribution of a λ dipole




• Fig. Current distribution of a $3\lambda/2$ dipole

Kinds of antennas

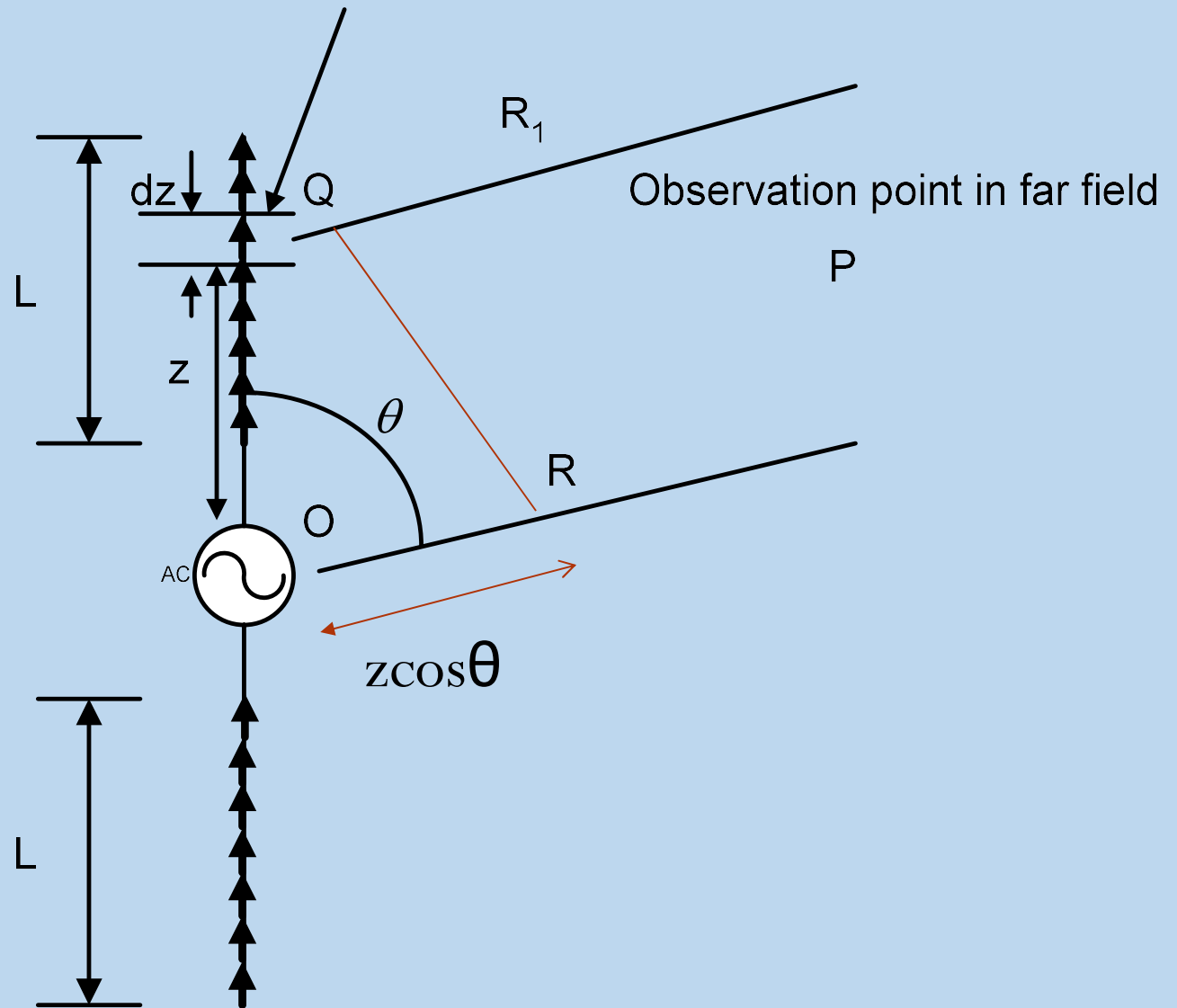
How to find the electric field?

- The electric field due to the current element dz
 - *it has the same expression of the Hertz dipole of the previous section*
 - *except that now we have a length of dz and current of $I(z)$*
- at far away observation point or in the *far field* can be written as

$$dE_{\theta} = \frac{j\beta^2 \sin \theta I(z) dz e^{-j\beta R_1}}{4\pi\epsilon_0 R_1}; dH_{\phi} = \frac{dE_{\theta}}{\eta_0}$$


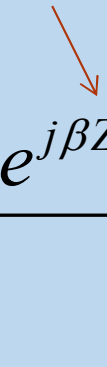
- Fig. (a) Dipole of length $2L$ (Dipole can be assumed to composed of many Hertz dipoles)

Equivalent to a Hertz dipole of length dz



Kinds of antennas

- Since the observation point P is at a very far distance, the lines OP and QP are parallel and therefore $\therefore R_1 \cong R - z \cos \theta$
- Note that for the amplitude, we can approximate $\frac{1}{R_1} \cong \frac{1}{R}$
 - since the dipole size is quite small in comparison to the distance of the observation point P from the origin
- Hence

$$dE_{\theta} \cong \frac{j\beta^2 \sin \theta I(z) dz e^{-j\beta R} e^{j\beta Z \cos \theta}}{4\pi\epsilon\omega R}$$


Kinds of antennas

- Since we have assumed that the dipole of length $2L$ is composed of many Hertz dipoles as depicted in Fig. (a)
 - (this is one of the reasons why we say that Hertz dipole or infinitesimal dipole is the building block for many antennas),
- we can write the total radiated electric field as

$$E_{\theta} = \int_{z=-L}^L dE_{\theta} = \int_{z=-L}^L \frac{j\beta^2 \sin \theta I(z) e^{-j\beta R} e^{j\beta Z \cos \theta}}{4\pi\epsilon\omega R} dz = \int_{z=-L}^L \frac{j\beta^2 \sin \theta I_0 \sin(\beta(L - |z|)) e^{-j\beta R} e^{j\beta Z \cos \theta}}{4\pi\epsilon\omega R} dz$$

Kinds of antennas

- It can be shown that (see textbook for derivations)

$$\Rightarrow E_{\theta} \cong \underbrace{j60I_0}_{\text{circled}} \frac{e^{-j\beta R}}{R} \left[\frac{\cos(\beta L \cos \theta) - \cos \beta L}{\sin \theta} \right] = j60I_0 \frac{e^{-j\beta R}}{R} F(\theta)$$


- In the previous equation,
 - the term under bracket is $F(\theta)$
 - and it is the variation of electric field as a function of θ and
- it is the E-plane radiation pattern

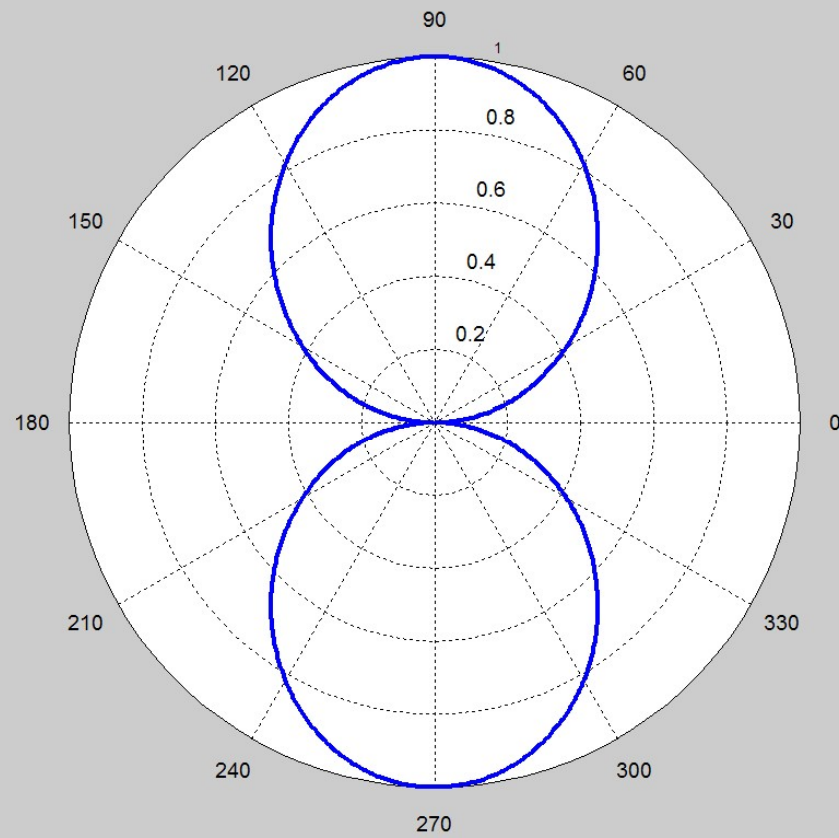
Kinds of antennas

- In the H-plane like that of Hertz dipole,
 - E_{θ} is a constant and it is not a function of ϕ
- hence it is a circle
- The E-plane radiation pattern of the dipole
 - varies with the length of the dipole as depicted in Fig.

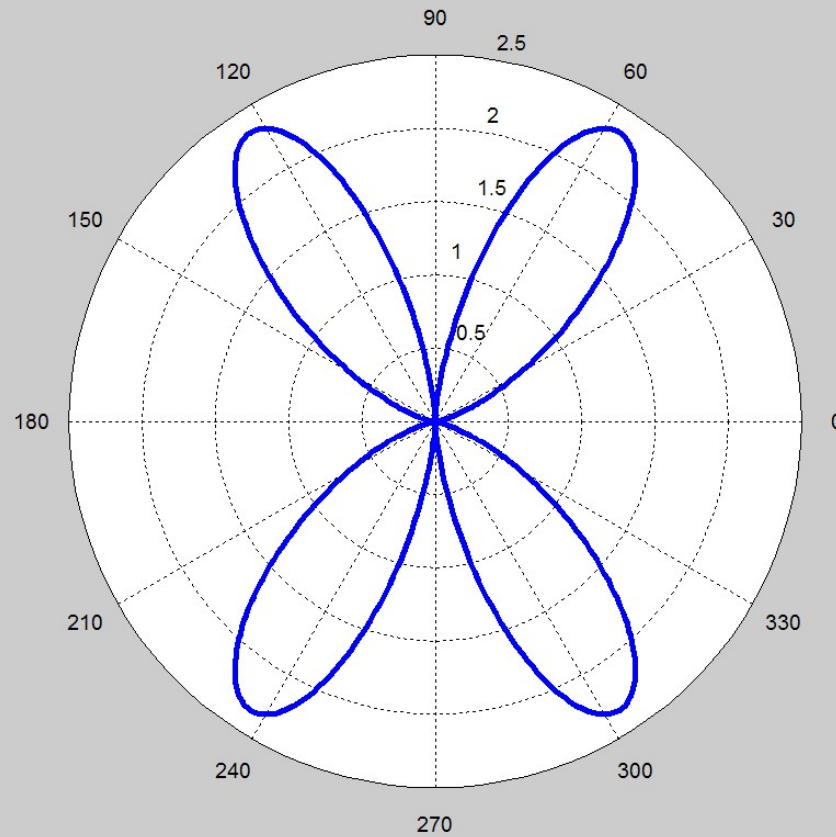
Kinds of antennas

- Note that
 - we have considered the total dipole length is $2L$
- Fig. E-plane radiation pattern for dipole of length
 - (a) $2L=2\times\lambda/4=\lambda/2$
 - (b) $2L=2\times\lambda=2\lambda$
 - (c) $2L=2\times2\lambda=4\lambda$

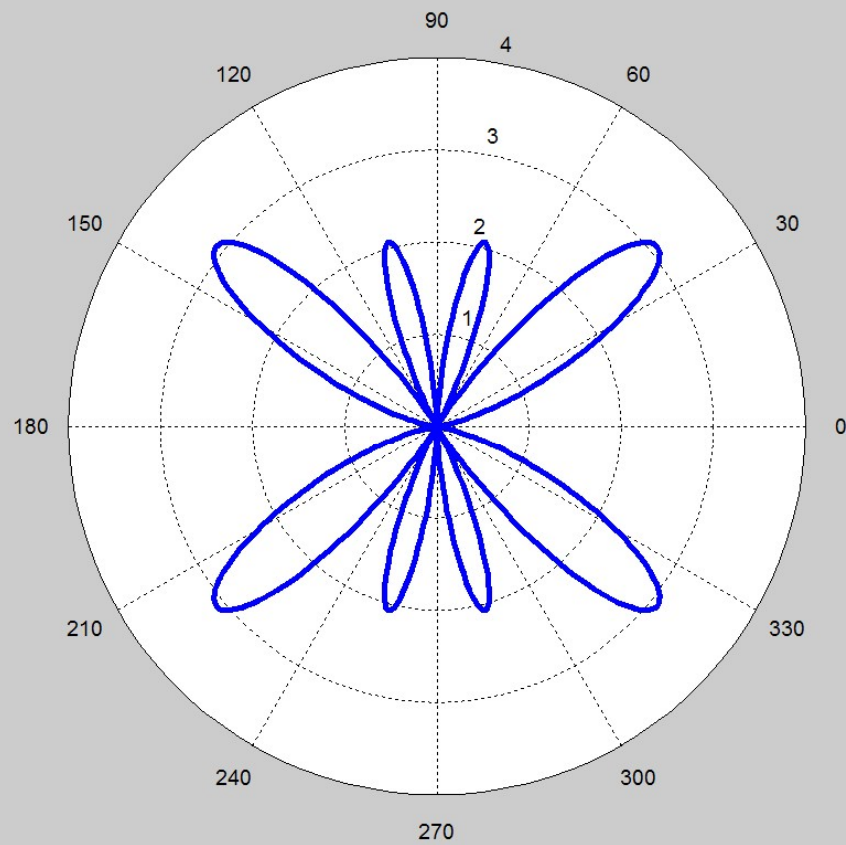
$$\Rightarrow E_{\theta} \cong j60I_0 \frac{e^{-j\beta R}}{R} \left[\frac{\cos(\beta L \cos \theta) - \cos \beta L}{\sin \theta} \right] = j60I_0 \frac{e^{-j\beta R}}{R} F(\theta)$$




- (a) $2L = 2 \times \lambda/4 = \lambda/2$



- (b) $2L = 2 \times \lambda = 2\lambda$



- (c) $2L = 2 \times 2\lambda = 4\lambda$

Kinds of antennas

Points to be noted:

1. Input impedance of the dipole ($z=0$, center of dipole)

$$Z_{in} = \frac{V_{in}}{I_{in}} = \frac{V_{in}}{I_0 \sin \beta L}$$

- For dipole of length $2L$, where $L = \text{odd multiples of } \frac{\lambda}{4}$, $\beta L = \frac{m\pi}{2}$, $\sin \beta L = 1$, $Z_{in} = \frac{V_{in}}{I_0}$
- For dipole of length $2L$, where $L = \text{even multiples of } \frac{\lambda}{4}$, $\beta L = m\pi$, $\sin \beta L = 0 \Rightarrow Z_{in} = \infty$

Kinds of antennas

- That's why
 - it is preferable to have dipoles of length odd multiples of $\lambda/2$,
 - otherwise
 - it is difficult to have a source with infinite impedance
2. Since increasing the dipole length more and more current is available for radiation,
- the total power radiated increases monotonically

Kinds of antennas

3. The electric field has only $\hat{\theta}$ component and hence it is linearly polarized
4. The radiation pattern have nulls and it can be calculated by equating $F(\theta)=0$

Kinds of antennas

$$\frac{\cos(\beta L \cos \theta_{null}) - \cos \beta L}{\sin \theta_{null}} = 0$$

$$\Rightarrow \cos \theta_{null} = \pm 1 \pm \frac{m\lambda}{\pi}$$

- For $m=0$, $\cos \theta_{null} = \pm 1, \theta_{null} = 0, \pi$
- But, in denominator $\sin \theta_{null}$ is also zero
- So let us take the limit of $F(\theta)$ as $\theta \rightarrow 0$, and see

Kinds of antennas

$$\begin{aligned} \lim_{\theta \rightarrow 0, \pi} \left\{ \frac{\cos(\beta L \cos \theta) - \cos(\beta L)}{\sin \theta} \right\} &\cong \lim_{\theta \rightarrow 0, \pi} \frac{1}{\sin \theta} \left[\left\{ 1 - \frac{(\beta L \cos \theta)^2}{2!} + \frac{(\beta L \cos \theta)^4}{4!} \right\} - \left\{ 1 - \frac{(\beta L)^2}{2!} + \frac{(\beta L)^4}{4!} \right\} \right] \\ &= \lim_{\theta \rightarrow 0, \pi} \left\{ \frac{(\beta L)^2 \sin^2 \theta}{2!} - \frac{(\beta L)^4 (1 - \cos^4 \theta)}{4!} \right\} \times \frac{1}{\sin \theta} = \lim_{\theta \rightarrow 0, \pi} \left\{ \frac{(\beta L)^2 \sin \theta}{2!} - \frac{(\beta L)^4 \sin \theta (1 + \cos^2 \theta)}{4!} \right\} = 0 \end{aligned}$$

5. To find θ for maximum radiation, we have to find the solution of

-

- $$\frac{dF(\theta)}{d\theta} = 0$$

- We can also take the mean of the first two nulls to approximate θ_{\max}

Kinds of antennas

- What is the radiation resistance of a dipole antenna?

$$R_r = \frac{2P_{rad}}{I_0^2}$$

- Radiated power can be obtained from the radiation intensity as

$$P_{rad} = \int_{\phi=0}^{2\pi} \int_{\theta=0}^{\pi} U(\theta, \phi) \sin \theta d\theta d\phi$$

Kinds of antennas

- Radiation intensity can be obtained from the Poynting vector

as

$$U(\theta, \phi) = r^2 S(\theta, \phi) = \frac{30}{\pi} I_0^2 |F(\theta)|^2$$

- For $\lambda/2$ dipole antenna

$$\because \beta L = \frac{2\pi}{\lambda} \times \frac{\lambda}{4} = \frac{\pi}{2}, \therefore F(\theta) = \frac{\cos(\beta L \cos \theta) - \cos(\beta L)}{\sin \theta} = \frac{\cos\left(\frac{\pi}{2} \cos \theta\right)}{\sin \theta}$$

- Therefore,

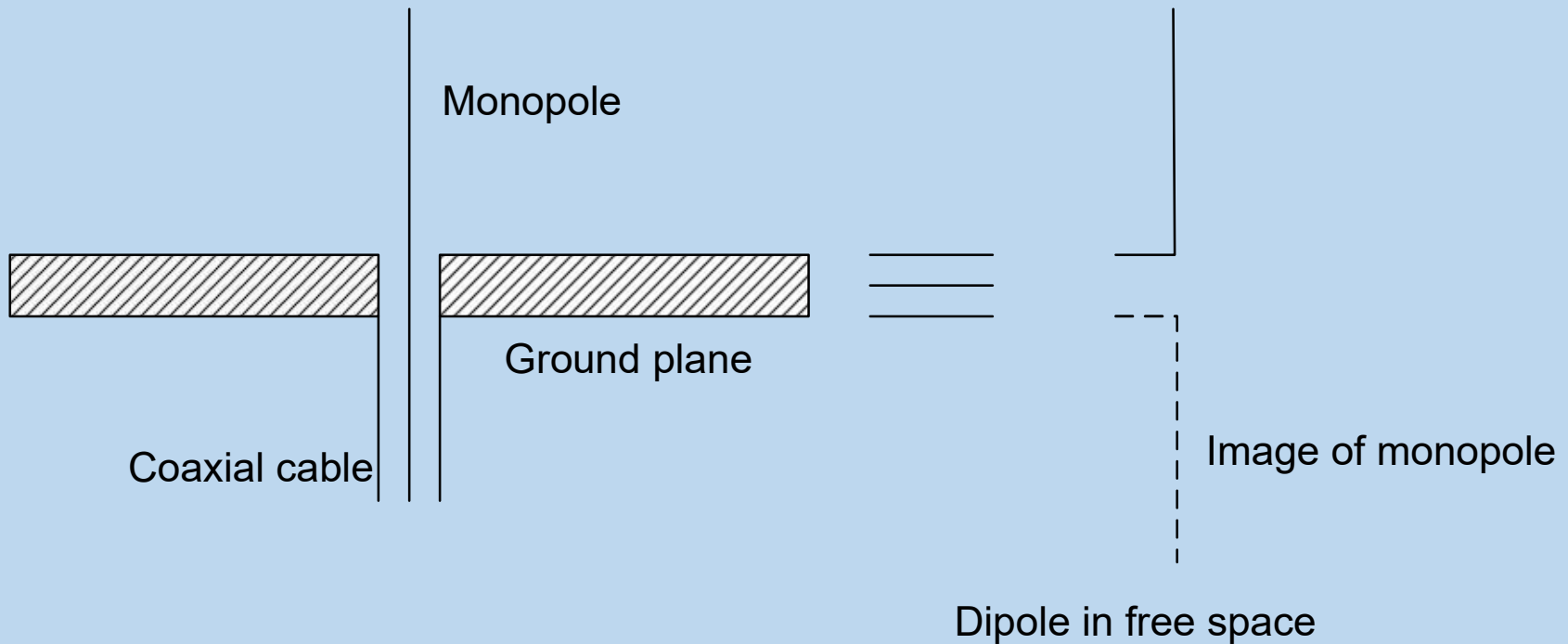
$$P_{rad} = \frac{30}{\pi} I_0^2 \int_{\theta=0}^{\pi} \frac{\cos^2\left(\frac{\pi}{2} \cos \theta\right)}{\sin^2 \theta} d\theta$$

Kinds of antennas

Monopole antennas:

- A monopole is a dipole that has been divided in half at its center feed point and
 - fed against a ground plane
- Monopole is usually fed from a coaxial cable (see Fig. (b))
- A monopole of length L placed above a perfectly conducting and infinite ground plane
 - will have the same field distribution to that of a dipole of length $2L$ without the ground plane

Kinds of antennas



- (b) Monopole of length L over a ground plane

Kinds of antennas

- This is because an image of the monopole will be formed inside the ground plane
 - (similar to the method of images)
- The monopole looks like a dipole in free space (see Fig. (b))
- Since this monopole is of length L only,
 - it will radiate only half of the total radiated power of a dipole of length $2L$
- Hence, the radiation resistance of a monopole is half that of a dipole

Kinds of antennas

- Similarly, directivity of the monopole is twice that of a dipole
- Since the field distributions are the same for a monopole and dipole,
 - the maximum radiation intensity will be also same for both cases
- But for monopole,
 - the total radiated power is half that of a dipole
- Hence, the directivity of a monopole above a conducting ground plane is
 - twice that of dipole in free space

Kinds of antennas

Loop antenna

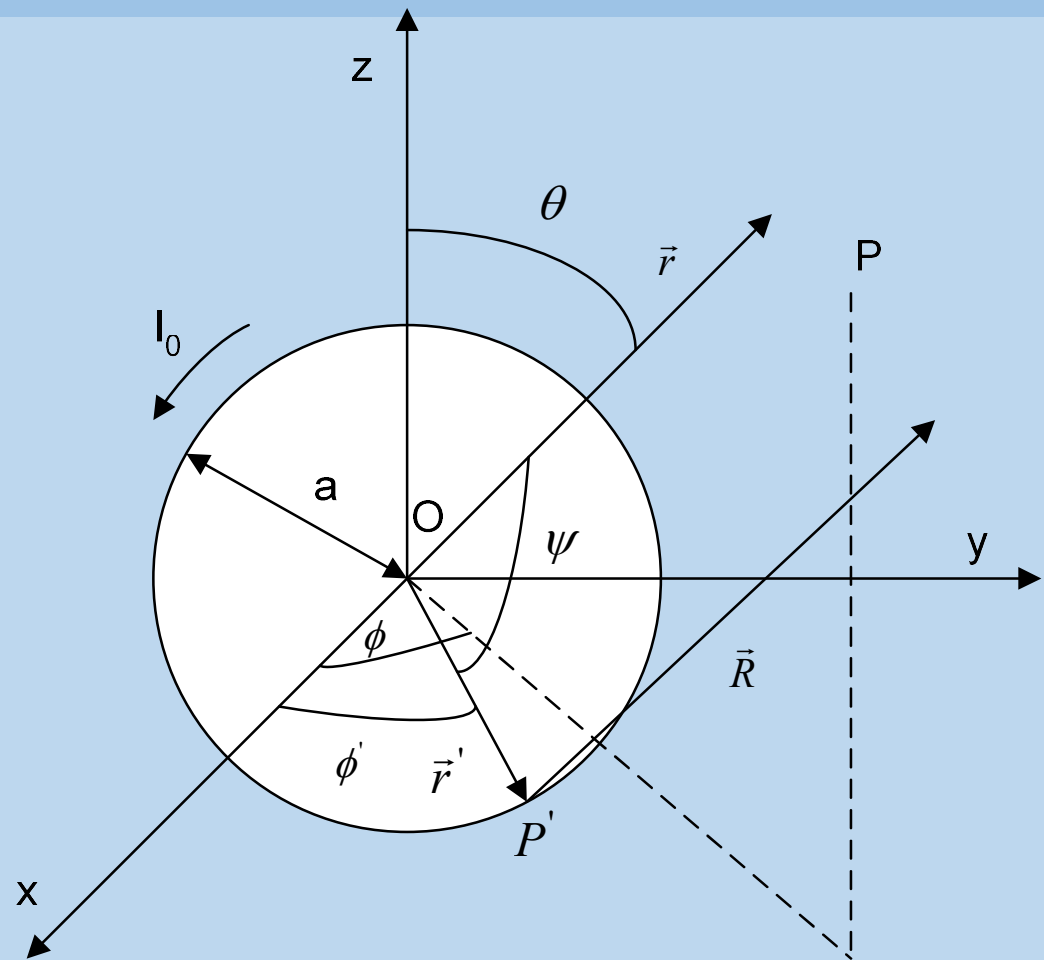
- Loop antennas could be of various shapes:
 - circular,
 - triangular,
 - square,
 - elliptical, etc.
- They are widely used in applications up to 3GHz
- Loop antennas can be classified into two:
 - electrically small (circumference $< 0.1 \lambda$) and
 - electrically large (circumference approximately equals to λ)

Kinds of antennas

- Electrically small loop antennas have
 - very small radiation resistance
- They have
 - very low radiation and
 - are practically useless
- Electrically small loop antennas could be analyzed assuming that
 - it is equivalently represented as a Hertz dipole
- Let us consider electrically large circular loop of constant current

Kinds of antennas

- Loop antenna



Kinds of antennas

- We can express magnetic vector potential (see textbook) as

$$A_{\phi}(\theta) = \frac{\mu I_0 a e^{-j\beta r}}{4\pi r} \pi j \{J_1(\beta a \sin \theta) - J_1(-\beta a \sin \theta)\}$$

$$\because J_n(z) = z^n \sum_{m=0}^{\infty} \frac{(-1)^m z^{2m}}{2^{2m+n} m!(n+m)!} \therefore J_n(-z) = (-1)^n J_n(z) \Rightarrow J_1(-\beta a \sin \theta) = -J_1(\beta a \sin \theta)$$

$$\therefore A_{\phi}(\theta) = \frac{j\mu I_0 a e^{-j\beta r} J_1(\beta a \sin \theta)}{2r}$$

- We can express electric field as

$$\therefore \vec{E} = -j \frac{\nabla(\nabla \cdot \vec{A})}{\omega\mu\epsilon} - j\omega\vec{A}$$

Kinds of antennas

- Note that magnetic vector potential has only ϕ component which is a function of θ variable only

$$\therefore \nabla \cdot \vec{A} = 0;$$

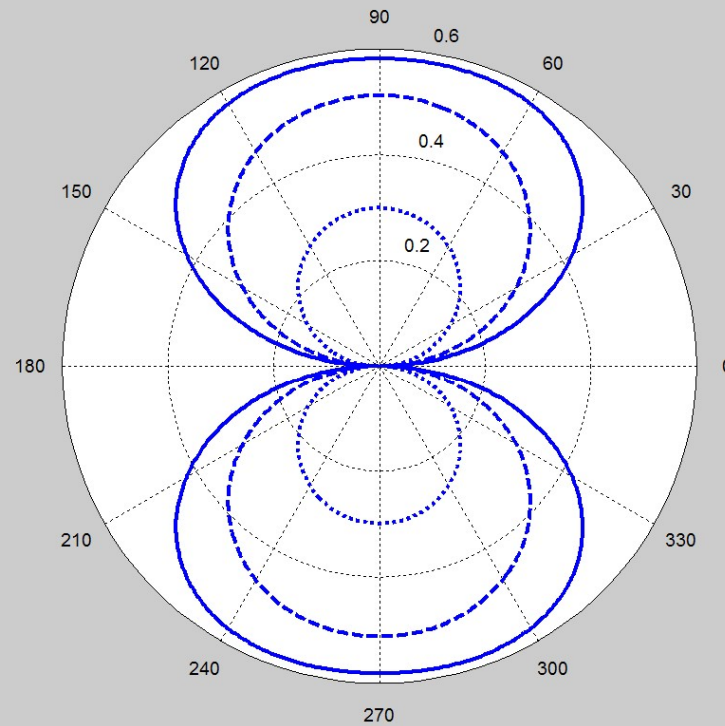
$$\because A_\theta = A_r = 0 \Rightarrow E_\theta = -j\omega A_\theta = 0; E_r = -j\omega A_r = 0 \therefore E_\phi = -j\omega A_\phi = \frac{\omega\mu I_0 a e^{-j\beta r} J_1(\beta a \sin \theta)}{2r}$$

$$H_\theta = -\frac{E_\phi}{\eta} = \frac{-\omega\mu I_0 a e^{-j\beta r}}{2\eta r} J_1(\beta a \sin \theta); H_r = H_\phi = 0$$

Kinds of antennas

- Poynting vector for a wave radiating in radially outward direction
 - should have direction along positive radial direction
- Therefore H_θ must be negative
- Fig. shows the far-field radiation pattern of the loop antenna
- It can be observed that the radiation field has higher magnitude
 - with the larger radius of the loop antenna
- For larger radiation power we need a loop antenna of larger radius

Kinds of antennas



- Fig. Plot of for various values of angle θ (far-field radiation patterns) (dotted line $\rightarrow a=0.1\lambda$, dashed line $\rightarrow a=0.2\lambda$, solid line $\rightarrow a=0.3\lambda$)

Kinds of antennas

- For small loops

$$\beta a < \frac{1}{3}; J_1(\beta a \sin \theta) = \frac{1}{2} \beta a \sin \theta - \frac{1}{16} (\beta a \sin \theta)^3 + \dots \cong \frac{1}{2} \beta a \sin \theta$$

$$\therefore E_\phi = \frac{\omega \mu I_0 a}{2} \frac{e^{-j\beta r}}{r} \frac{1}{2} (\beta a \sin \theta); H_\theta = -\frac{\omega \mu I_0 a}{\eta} \frac{e^{-j\beta r}}{2r} \frac{1}{2} (\beta a \sin \theta)$$

- Note that for the dipole polarization was along $\hat{\theta}$ direction
- But for small loop antennas it is along the $\hat{\phi}$ direction