EE540 Advance Electromagnetic Theory & Antennas

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• Fig. Boundary for electric fields at the interface of two media (Interface at z=0, z>0 is region 1 and z<0 is region 2)

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• Use Faraday's law over loop PQRSP (LHS), note that loop PQRSP is in x-y plane

 $\oint_C \vec{E} \bullet d\vec{l} = -\iint_S \left(\frac{\partial \vec{B}}{\partial t}\right) \bullet d\vec{s}$

- Note that $h \rightarrow 0$ at the boundary interface and
- therefore there is no contribution from
 - QR and SP in the above line integral
- Also note that the direction of the line integral along
 - PQ and RS are in the opposite direction

$$\therefore \oint_{PQRSP} \vec{E} \bullet d\vec{l} = \int_{P}^{Q} \vec{E}_1 \bullet d\vec{l}_1 + \int_{R}^{S} \vec{E}_2 \bullet d\vec{l}_2 = E_{1t}l - E_{2t}l$$

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• Use Faraday's law over surface PQRS (RHS)

$$\vec{E} \bullet d\vec{l} = -\int_{S} \left(\frac{\partial B}{\partial t} \right) \bullet d\vec{s}$$

- If time and space dependence of \vec{B} are independent
- We can take the time derivative outside the integral

$$\oint_{C} \vec{E} \bullet d\vec{l} = -\frac{\partial}{\partial t} \int_{S} \vec{B} \bullet d\vec{s}$$

- Also area of PQRS is small enough that \vec{B} is same w.r.t. space
- We can take the \vec{B} outside the integration

$$\oint_C \vec{E} \bullet d\vec{l} = -\frac{\partial}{\partial t} \left(\vec{B} \bullet \int_S d\vec{s} \right) = -\frac{\partial}{\partial t} \left(\vec{B} \bullet \vec{S} \right)$$

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Boundary conditions for electric fields

- Let us denote area of PQRS by A_{PQRS} and its direction will be normal to the surface i.e. along \hat{z}

$$\oint_{C} \vec{E} \bullet d\vec{l} = -\frac{\partial}{\partial t} \left(\vec{B} \bullet \vec{S} \right) = -\frac{\partial \left(\vec{B} \bullet \hat{z} A_{PQRS} \right)}{\partial t}$$

- We have the area of PQRS, $A_{PQRS} = lh$, hence $\oint_{C} \vec{E} \bullet d\vec{l} = -\frac{\partial (\vec{B} \bullet \hat{z} lh)}{\partial t} = -\frac{\partial (B_{z} lh)}{\partial t}$
- Note that $h \rightarrow 0$, area of PQRS, $A_{PQRS} \rightarrow 0$
- So RHS surface integral is negligible, therefore

 $E_{1t}l - E_{2t}l = 0 \Longrightarrow E_{1t} = E_{2t}$

• First boundary condition of electric field

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- Boundary conditions for electric flux density
- (Second boundary condition of electric field) $\oint \vec{D} \bullet d\vec{s} = \int \rho_v dv$
 - Let us consider a small cylinder at the interface
 - Cross section of the cylinder must be such that
 - vector \vec{D} is the same
- Note that h→0 at the boundary interface at z=0 (use cylindrical coordinate, z>0 is region 1 and z<0 is region 2)
 - therefore, there are no contribution from the curved surface of the pillbox in the above surface integral
- So only the top and bottom surfaces remains in the surface integral

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Boundary conditions for electric fields

$$\oint \vec{D} \bullet d\vec{s} = \int \vec{D}_2 \bullet d\vec{s}_2 + \int \vec{D}_1 \bullet d\vec{s}_1 = Q_{enclosed}$$
villbox top surface bottom surface

- The normal is in the upward direction in the top surface
- and downward direction in the bottom surface
- $D_{2n}\Delta S D_{1n}\Delta S = \rho_s \Delta S$
- $D_{2n} D_{1n} = \rho_s$
- the normal component of electric flux density
 - can only change at the interface
- if there is charge on the interface, i.e.,
 - surface charge is present

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Boundary conditions for magnetic fields

• Use Modified Ampere's law over loop PQRSP (LHS)

 $\oint_C \vec{H} \bullet d\vec{l} = \int_S \left(\vec{J} + \frac{\partial \vec{D}}{\partial t}\right) \bullet d\vec{s}$

- Note that $\Delta h \rightarrow 0$ at the boundary interface and
- therefore there is no contribution from
 - QR and SP in the above line integral
- Also note that the direction of the line integral along
 - PQ and RS are in the opposite direction

$$\therefore \oint_{PQRSP} \vec{H} \bullet d\vec{l} = \int_{P}^{Q} \vec{H}_{1} \bullet d\vec{l}_{1} + \int_{R}^{S} \vec{H}_{2} \bullet d\vec{l}_{2} = H_{1t}l - H_{2t}l$$

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Boundary conditions for magnetic fields

Use Modified Ampere's law over surface PQRS (RHS)

$$\vec{H} \bullet d\vec{l} = \int_{S} \left(\vec{J} + \frac{\partial D}{\partial t} \right) \bullet d\vec{s}$$

- If time and space dependence of \vec{D} are independent
 - Also area of PQRS is small enough that \vec{D} is same w.r.t. space

$$\oint_{C} \vec{H} \bullet d\vec{l} = \int_{S} \vec{J} \bullet d\vec{s} + \frac{\partial}{\partial t} \int_{S} \vec{D} \bullet d\vec{s} = \int_{S} \vec{J} \bullet d\vec{s} + \frac{\partial \left(\vec{D} \bullet \vec{J} \cdot \vec{ds}\right)}{\partial t} = \int_{S} \vec{J} \bullet d\vec{s} + \frac{\partial \left(\vec{D} \bullet \vec{S}\right)}{\partial t}$$
$$\Rightarrow \oint_{C} \vec{H} \bullet d\vec{l} = \int_{S} \vec{J} \bullet d\vec{s} + \frac{\partial \left(\vec{D} \bullet \hat{z}(\Delta hl)\right)}{\partial t} = \int_{S} \vec{J} \bullet d\vec{s} + \frac{\partial \left(D_{z}(\Delta hl)\right)}{\partial t}$$

- Note that $\Delta h \rightarrow 0$, area of PQRS, $A_{PQRS} \rightarrow 0$
- So the 2nd term of RHS surface integral is negligible, so

$$\oint_C \vec{H} \bullet d\vec{l} = \int_S \vec{J} \bullet d\vec{s} + 0$$
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Boundary conditions for magnetic fields

- Note that \vec{J} here is volume current density due to free charge
- Maxwell's equations we have considered is for
 - free charge and current density
 - volume current density is often referred to as current density
- What is volume current density?
- It is the amount of current passing through a unit area
 - *normal/perpendicular* to the direction of current flow
 - Its unit is A/m²
- Volume current density at a point \vec{r} is defined as
 - In other words you may consider ΔS perpendicular
 - to the current flow

 $\vec{J}(\vec{r}) = \frac{\lim}{\Delta S^{\perp} \to 0} \frac{\Delta I}{\Delta S^{\perp}} \hat{n} \left(A/m^2 \right)$

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Fig. Definition of volume current density (assume \hat{n} is normal to surface element ΔS and current ΔI is flowing in that direction)

भारतीय प्रौद्योगिकी संस्थान गुवाहाटी INDIAN INSTITUTE OF TECHNOLOGY GUWAH Boundary conditions for magnetic fields

- What is surface current density?
- Surface current density is the amount of current passing through a unit width
 - normal/perpendicular to the direction of current flow
 - Its unit is A/m
- Alternate way of looking at surface current density
 - Consider current flow in a thin layer
 - Imagine you squeeze the height of the surface element
 - considered perpendicular to the current flow
 - to zero ($\Delta h \rightarrow 0$), then it will form a line of length Δl^{\perp}
- In this case, we can consider a surface current density
- It is defined at a point \vec{r} as

$$\vec{J}_{S}(\vec{r}) = \frac{\lim}{\Delta l^{\perp} \to 0} \frac{\Delta I}{\Delta l^{\perp}} \hat{n} (A/m)$$

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Fig. Definition of surface current density (assume Δl^{\perp} is perpendicular to the flow of current and Δl is the current flowing)

Current ΔI

Δh



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Boundary conditions for magnetic fields Note that for small area of PQRS J (volume current density) remains the same within PQRS

$$\oint_C \vec{H} \bullet d\vec{l} = \int_S \vec{J} \bullet d\vec{s} = \vec{J} \bullet \int_S d\vec{s} = \vec{J} \bullet \vec{S} = \vec{J} \bullet \Delta h l\hat{z} = (\vec{J} \Delta h) \bullet l\hat{z}$$

• When $\Delta h \rightarrow 0$, we can define

$$\lim_{\Delta h \to 0} \vec{J} \Delta h = \vec{J}$$

- We call this impressed surface electric current density $\vec{I_s}$ at the interface
 - and its unit will be A/m
- Hence RHS after noting that $\vec{J_S}$ is along \hat{z} direction, we will now have $\oint \vec{H} \bullet d\vec{l} = (\vec{J}_S) \bullet l\hat{z} = (J_S)\hat{z} \bullet l\hat{z}$
- Therefore.

$$H_{1t}l - H_{2t}l = J_S l \Longrightarrow H_{1t} - H_{2t} = J_S$$

First boundary condition of magnetic field

Fig. Illustration of volume and surface current density and its equivalence with current *I* ($I = (I\Delta h)\Delta l^{\perp} = I_S\Delta l^{\perp}$)

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$$\Delta w$$

$$J$$



Boundary conditions for magnetic fields

- Boundary conditions for magnetic flux density
- (Second boundary condition of magnetic field) $\oint \vec{B} \bullet d\vec{s} = 0$
 - Let us consider a^ssmall cylinder at the interface
 - Cross section of the cylinder must be such that
 - vector \vec{B} is the same
- Note that $\Delta h \rightarrow 0$ at the boundary interface
 - therefore, there are no contribution from the curved surface of the pillbox in the above surface integral
- So only the top and bottom surfaces remains in the surface integral



Boundary conditions for magnetic fields

$$\oint_{pillbox} \vec{B} \bullet d\vec{s} = \int_{top} \vec{B}_2 \bullet d\vec{s}_2 + \int_{bottom} \vec{B}_1 \bullet d\vec{s}_1 = 0$$

- The normal is in the upward direction in the top surface
- and downward direction in the bottom surface
- $B_{2n}\Delta S B_{1n}\Delta S = 0$
- $B_{2n} = B_{1n}$
- the normal component of magnetic flux density
 - are continuous at the boundary

Boundary conditions for current density



Fig. Boundary conditions for current density

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Boundary conditions for current density

- Let us construct a pillbox
 - whose height is so small that the contribution from the
 - curved surface of the cylinder to the current can be neglected
- Applying equation of continuity
 - points with changing ho_{v} is the source for current density
 - for steady state (there are no points with changing ho_{v} w.r.t. time)

$$i = -\frac{dq}{dt} = -\frac{d}{dt} \left(\int_{V} \rho_{v} dv \right) \Longrightarrow \oint_{S} \vec{j} \bullet d\vec{s} = -\frac{d}{dt} \left(\int_{V} \rho_{v} dv \right)$$

• and computing the surface integrals, we have,

$$i = \oint_{S} \vec{j} \bullet d\vec{s} = 0 \Rightarrow \hat{n} \bullet \vec{J}_{1} \Delta s - \hat{n} \bullet \vec{J}_{2} \Delta s = 0 \Rightarrow \hat{n} \bullet \left(\vec{J}_{1} - \vec{J}_{2}\right) = 0 \Rightarrow J_{n1} = J_{n2}$$
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Boundary conditions for current density

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- It states that the normal component
 - of electric current density is
 - continuous across the boundary
- Since, we have another boundary condition
 - that the tangential component of the
 - electric field is continuous across the boundary,
 - and applying Ohm's law in point form $\vec{J} = \sigma \vec{E}$
- We have,

$$\widehat{n} \times \left(\vec{E}_1 - \vec{E}_2\right) = 0 \Longrightarrow \widehat{n} \times \left(\frac{\vec{J}_1}{\sigma_1} - \frac{\vec{J}_2}{\sigma_2}\right) = 0 \Longrightarrow \frac{J_{t1}}{\sigma_1} - \frac{J_{t2}}{\sigma_2} = 0 \Longrightarrow \frac{J_{t1}}{J_{t2}} = \frac{\sigma_1}{\sigma_2}$$

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